

THE APPLICATION OF EXTENDED
KALMAN FILTERING TO THE
POSITION LOCATING REPORTING SYSTEM (PLRS)

Charles A. Dittmar

DUDLEY KNOX LIBRARY
NAVAL POSTGRADUATE SCHOOL
MONTEREY, CALIFORNIA 93940

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

THE APPLICATION OF EXTENDED
KALMAN FILTERING TO THE
POSITION LOCATING REPORTING SYSTEM (PLRS)

by

Charles A. Dittmar, Jr.

December 1975

Thesis Advisor:

H.A. Titus

Approved for public release; distribution unlimited.

Prepared for:
Naval Electronics System Command
Washington, D.C. 22030

T173026

NAVAL POSTGRADUATE SCHOOL
Monterey, California

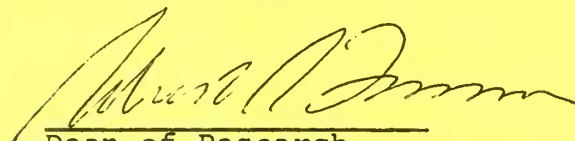
Rear Admiral Isham Linder
Superintendent

Jack R. Borsting
Provost

This thesis prepared in conjunction with research supported in part by Naval Electronics System Command under Project Number N0003975PO52945.

Reproduction of all or part of this report is authorized.

Released as a
Technical Report by:


Dean of Research

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NPS-52TS75121	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) The Application of Extended Kalman Filtering to the Position Locating Reporting System (PLRS)		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; December 1975
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Charles A. Dittmar, Jr.		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		12. REPORT DATE December 1975
		13. NUMBER OF PAGES 79
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Research supported in part by Naval Electronics System Command under Project Number N0003975PO52945.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) PLRS Position Locating Reporting System Extended Kalman filtering		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Extended Kalman filtering is applied to the PLRS (Position Locating Reporting System). Here the nonlinearity to the filter enters through the measurement (range only). The nonlinearity being the relationship between range and the cartesian coordinate states of the filter. Filter covariances of error are portrayed as error ellipsoids. These are used to determine which one		



(20. ABSTRACT Continued)

should be used to update a unit when there are several other units available for ranging. One should attempt to make the range measurement in the same direction as the major axis of error associated with the unit to be updated.

The filtering techniques are evaluated using static units and high speed maneuvering aircraft.

The Application of Extended Kalman Filtering to the
Position Locating Reporting System(PLRS)

by

Charles A. Dittmar, Jr.
Captain, United States Marine Corps
B.S., United States Naval Academy, 1968

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
December 1975

ABSTRACT

Extended Kalman filtering is applied to the PLRS (Position Locating Reporting System). Here the nonlinearity to the filter enters through the measurement (range only). The nonlinearity being the relationship between range and the cartesian coordinate states of the filter.

Filter covariances of error are portrayed as error ellipsoids. These are used to determine which one should be used to update a unit when there are several other units available for ranging. One should attempt to make the range measurement in the same direction of the major axis of error associated with the unit to be updated.

The filtering techniques are evaluated using static units and high speed maneuvering aircraft.

TABLE OF CONTENTS

I.	INTRODUCTION -----	8
II.	POSITION LOCATING PROBLEM -----	11
	A. THE FILTER'S DYNAMIC MODEL OF AIRCRAFT UNITS -----	11
	B. EXTENDED KALMAN FILTER -----	12
III.	RANGE MEASUREMENT PROCESSING AND ERROR ELLIPSOIDS -----	17
IV.	TRACKING AND MANEUVERING TARGETS -----	26
	A. THE CHOICE OF Q -----	26
	B. SIMULATION RESULTS -----	27
V.	CONCLUSIONS -----	39
	APPENDIX. COMPUTER PROGRAM -----	40
	LIST OF REFERENCES -----	78
	INITIAL DISTRIBUTION LIST -----	79

LIST OF FIGURES

1. Error ellipsoids for two fixed units displaced along y-axis 15 KM ----- 20
2. Projection of error ellipsoids to their x-y components and updated error ellipsoids after each unit ranges on the other ----- 21
3. Sequential updating of the units, one upon the other, over ten observations ----- 25
4. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging only on unit #2.
x = true track, o = noise track, + = filter track -- 31
5. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging on unit #2 and unit #1 during second half.
x = true track, o = noise track, + = filter track -- 32
6. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working poorly in last third of flight (unit #1 ranges solely on last 20 observations. A too low Q is indicated by the track bias.
x = true track, o = noise track, + = filter track -- 33
7. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 10 M.
x = true track, o = noise track, + = filter track -- 34
8. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 100 M.
x = true track, o = noise track, + = filter track -- 35
9. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Filter drops track due to extreme measurement noise (1 KM).
x = true track, o = noise track, + = filter track -- 36

10. Aircraft in circular track at Mach 1 and radius of 10 KM. Error ellipsoids presented on every fifth observation. Measurement noise = 10 M. Switching algorithm fails on x-axis. Ellipses 25 times true scale.
x = true track, \square = noise track, + = filter track -- 37
11. Aircraft in circular track at Mach 1 and radius of 10 KM. Switching algorithm corrected. Ellipses 25 times true scale.
x = true track, \square = noise track, + = filter track -- 38

I. INTRODUCTION

Position location of tactical elements in the Marine Corps in the past has relied upon the fact that these units had maps from which they could determine their position. Position determination is therefore highly dependent on the ability of an individual to correctly orient himself to the natural terrain surrounding him and locate this same terrain on the map. Once located, the requirement then exists to transmit position information via radio link to parent units. Meshed with the ground commander's problem of position location is the task of organizing and conducting support operations such as medical evacuation of wounded personnel, artillery, naval gunfire and air support.

Using visual references it becomes difficult to accurately locate one's position when operating in mountainous terrain, in heavy vegetation, at night or in bad weather. And with the heavy volume of radio traffic experienced during battle, the probability of communicating to higher headquarters a unit's position or information about that position is reduced. As a result the support operations mentioned earlier are delayed because of detailed clearances required to ensure protection of friendly units whose position is not precisely known.

The obstacles to position location suggested can and do arise in the conduct of actual operations, and for that

reason, the Marine Corps has written specifications detailing a Position Location and Reporting System (PLRS) designed for tactical employment on the battlefield, [1]. The system as construed is to consist of a containerized master unit composed of a general purpose computer and communications control electronics. This unit is referred to as the Master Unit. It is responsible for processing all range information inputs to the system, and displaying unit positions on a visual display with a variety of other information.

The other units in the area are all portable, capable of being carried by a single man, vehicle, or aircraft. They are referred to as update or ranging units depending on their particular function at the time. When a unit's position is being improved, that unit is referred to as the "update" unit. All other units that are in contact with the update unit and are providing range measurements are "ranging" units. The frequency at which each unit is updated is specified according to its type. That is, aircraft traveling at much higher velocities than men will require updates more often if their tracking is to be accurate.

Before a unit can be tracked and position estimates made, an initial estimate of position must be made. This process of initialization is controlled by the master unit. Once a unit is initialized the computer systematically selects ranging units processing their associated range information as applicable. In processing range information a new position estimate and a measure of the uncertainty in the estimate is provided.

While the processing of accumulated range information for an update unit appears to be straightforward, the difficulty lies in deciding which ranges to process so that the most accurate position estimates will be obtained. Range information is a measurement of the time required to send a signal from the ranging unit to the update unit and back again plus some built in delays.

While the measurement of times associated with the total time is quite accurate, it is still subject to the effects of noise therefore range is a noisy measurement. In addition the uncertainty of the ranging unit's position adds to the uncertainty of the measurement itself. Therefore the selection of a ranging unit to best update a particular unit becomes a very important factor in the position location problem. One would desire to use the ranging unit nearest the line of the major axis of error in the unit to be updated.

The error ellipsoids of the "update" and "ranging" units and their relative geometry are analyzed and their influence on the tracking is portrayed in examples with maneuvering high speed aircraft and with stationary units.

II. POSITION LOCATING PROBLEM

A. THE FILTER'S DYNAMIC MODEL OF AIRCRAFT UNITS

First consider units in aircraft in a two dimensional space.* The estimate that we seek in this problem is position (X,Y) and velocity, (\dot{X},\dot{Y}) . X and Y are calculated with respect to a relative grid at a point on the earth's surface. The altitude is the vertical height above the earth at that particular XY grid intersection, and is not utilized in this investigation.

For tracking we may choose a fourth order state vector,

$$\underline{x} = \begin{bmatrix} X \\ \dot{X} \\ Y \\ \dot{Y} \end{bmatrix} \quad (1)$$

Writing the equations in linear state form results in

$$\underline{x}(k+1) = \Phi \underline{x}(k) + \Gamma \underline{w}(k) \quad (2)$$

where

$$\Phi = \begin{bmatrix} 1 & T & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & T \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (3)$$

*The altitude tracking will be handled independently.

and

$$\Gamma = \begin{bmatrix} \frac{T^2}{2} & 0 \\ T & 0 \\ 0 & \frac{T^2}{2} \\ 0 & T \end{bmatrix} \quad (4)$$

B. EXTENDED KALMAN FILTER

The observable range is a nonlinear function of the states. So we must briefly look at how the nonlinearities can be handled in this type of problem.

Consider a nonlinear discrete system of state and observation equations given by

$$\underline{x}(k+1) = \underline{f}(\underline{x}(k), k) + \underline{g}(\underline{x}(k), k) \cdot \underline{w}(k) \quad (5)$$

and

$$\underline{z}(k) = \underline{h}(\underline{x}(k), k) + \underline{v}(k) \quad (6)$$

In these equations \underline{f} , \underline{g} and \underline{h} are nonlinear functions of the state variables \underline{x} , $\underline{w}(k)$ is plant excitation noise, and $\underline{v}(k)$ is measurement noise. The plant noise and measurement noise are assumed uncorrelated, zero-mean, and white. That is

$$E[\underline{w}(k) \cdot \underline{w}^T(j)] = Q'(k) \delta_{kj}$$

and

$$E[\underline{v}(k) \cdot \underline{v}^T(j)] = R(k) \delta_{kj}$$

In order to apply the linear filter equations, (5) and (6) are expanded about the best estimate of the state at that time and only the first-order terms are kept. Equation (5) gives

$$\underline{x}(k+1) = \Phi(k) \underline{x}(k) + \Gamma(k) \cdot \underline{w}(k) , \quad (7)$$

with

$$\Phi(k) = \left. \frac{\partial \underline{f}}{\partial \underline{x}} \right|_{\underline{x}=\hat{\underline{x}}(k)} .$$

Similarly Eq. (6) yields

$$\underline{z}(k) = H(k) \underline{x}(k) + \underline{v}(k) \quad (8)$$

where

$$H(k) = \left. \frac{\partial h}{\partial \underline{x}} \right|_{\underline{x}=\underline{x}'(k)} . \quad (9)$$

$\hat{\underline{x}}(k)$ is the estimated state value after the k^{th} measurement and $\underline{x}'(k)$ is the predicted value of the state before the k^{th} measurement. That is,

$$\underline{x}'(k) = \underline{f}(\underline{\hat{x}}(k-1), k-1) \quad . \quad (10)$$

A state error vector is defined by

$$\underline{\tilde{x}}(k) = \underline{\hat{x}}(k) - \underline{x}(k) \quad ,$$

and a predicted state error vector is defined by

$$\underline{\tilde{x}}'(k) = \underline{x}'(k) - \underline{x}(k) \quad .$$

The covariance of state error matrix is defined by

$$P(k) = E[\underline{\tilde{x}}(k) \cdot \underline{\tilde{x}}^T(k)] \quad ,$$

and the predicted covariance of state error matrix is given by

$$P'(k) = E[\underline{\tilde{x}}'(k) \cdot \underline{\tilde{x}}'^T(k)] \quad .$$

The state excitation matrix is given by

$$Q(k) = E[\Gamma(k) \cdot \underline{w}(k) \cdot \underline{w}^T(k) \cdot \Gamma^T(k)] \quad ,$$

and the measurement noise covariance matrix is

$$R(k) = E[\underline{v}(k) \cdot \underline{v}^T(k)] \quad .$$

The Kalman Filter equations are given by [2]

$$P'(k+1) = \Phi(k)P(k)\Phi^T(k) + Q(k) \quad (11)$$

$$G(k) = P'(k)H^T(k) [H(k)P'(k)H^T(k) + R(k)]^{-1} \quad (12)$$

$$P(k) = [I - G(k)H(k)] P'(k) \quad (13)$$

$$\underline{x}'(k) = \underline{f}(\underline{\hat{x}}(k-1), k) \quad (14)$$

$$\underline{z}'(k) = \underline{h}(\underline{x}'(k), k) \quad (15)$$

$$\underline{\hat{x}}(k) = \underline{x}'(k) + G(k) [\underline{z}(k) - \underline{z}'(k)] \quad (16)$$

The Q matrix serves not only to allow for maneuvering but also to account for any model inaccuracies. That is, any discrepancies between the true action of the physical system and its characterization by Eq. (7). For a filter which reaches steady-state conditions the Q also serves to prevent the gain matrix G(k) from approaching zero by always insuring uncertainty in the predicted covariance of error matrix P'(k).

The observation equation is nonlinear in the states and is given by

$$z(k) = [x(k)^2 + y(k)^2]^{1/2} \quad (17)$$

Equation (9) can be used to give observation matrix. The result is

$$H(k) = \begin{bmatrix} \frac{x(k)}{x(k)^2 + y(k)^2} & 0 & \frac{y(k)}{x(k)^2 + y(k)^2} & 0 \end{bmatrix} \quad (18)$$

In doing this, the recursive Kalman filter equations have been extended to cover the nonlinear case. The pseudo measurement matrix, H , must now be calculated from the position estimates at each time interval.

The use of the Extended Kalman technique in tracking a unit as it moves through the area presents a unique problem. Because we are observing only the range, we can improve our estimate of location only along the direction of the range vector. That is, the uncertainty or error variance in location remains unchanged in cross-range. We must then choose another ranging unit nearby that will improve upon this cross range error. This however is done later at the next prescribed interval for update of the unit in question.

The conclusion drawn from this observation is that it is critical that an algorithm be developed for selecting the best observations (ranging units) to process in the updating of a unit. It will be shown that this algorithm must be dependent on the physical geometry associated with the covariance error ellipses. It takes into consideration the error covariances associated with both the update and ranging units.

III. RANGE MEASUREMENT PROCESSING AND ERROR ELLIPSOIDS

The position of each unit within the system is established with a degree of uncertainty about the estimate. This uncertainty is expressed in the covariance of error matrix, P , and represents the sigma squared error deviation about the estimate. The position diagonal terms (P_{11} and P_{33}) of the covariance matrix represent the variances of the estimate in the XY coordinate directions. Their respective off diagonal terms (covariances) represent the degree of coupling and the orientation of the uncertainty in the XY plane.

If the errors were normally distributed, there exists a rotated coordinate system such that in the new system the orthogonal position components are uncorrelated. This is equivalent to taking the exponent of the joint normal probability density function, and applying a coordinate transformation which eliminates the cross terms.

The exponent (for zero-mean random variables) is

$$\frac{x^2}{\sigma_x^2} - \frac{2r_{xy}xy}{\sigma_x\sigma_y} + \frac{y^2}{\sigma_y^2} . \quad (19)$$

When set equal to a constant, this curve, which is an ellipse, is a curve of constant probability. This ellipse does not have its major and minor axes aligned with the coordinate system however. By applying the transformation

$$x' = x \cos \theta + y \sin \theta \quad (20)$$

and

$$y' = y \cos \theta - x \sin \theta \quad (21)$$

with

$$\theta = \frac{1}{2} \tan^{-1} \left[\frac{2 \operatorname{cov}(x,y)}{\sigma_x^2 - \sigma_y^2} \right], \quad (22)$$

the ellipse will be aligned with the x' , y' axis and the resultant random variables will be uncorrelated. The new variances in this system are calculated by

$$\sigma_{x'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} + \frac{\operatorname{cov}(xy)}{\sin 2\theta}, \quad (23)$$

and

$$\sigma_{y'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} - \frac{\operatorname{cov}(xy)}{\sin 2\theta}. \quad (24)$$

This method of viewing the sample statistics provides insight into the filter performance because it shows the regions of high probability and their geometric relationships. The values of $\sigma_{x'}^2$ and $\sigma_{y'}^2$ are referred to as the rotated error variances in the following section.

When a range measurement is made between two units, each with a different and independent error ellipse, the uncertainty of position along the range line connecting the two is improved for both units. In addition, it is sometimes possible to reduce the error of the axis orthogonal to the range line depending on the orientation of the error ellipse.

To study the influence of the error ellipsoids of the ranging and update unit let us consider a static example. This model is synonymous with those used for foot soldiers.

Measurement noise will be considered to come solely from the error variance of the ranging unit and vice versa when their roles interchanged. That is, at the same time the "update" unit is being updated, let us also update the "ranging" unit. The estimates of position and their error ellipsoids are shown in Fig. 1.

A projection of the error ellipsoid along the y-axis is given in Fig. 2. If one utilizes each as an observation to update the other, the resulting variance of both along the range line is given by

$$\sigma_{\text{new}}^2 = \frac{\sigma_1^2 \sigma_2^2}{\sigma_1^2 + \sigma_2^2}$$

where σ_1 and σ_2 are the standard deviations of units 1 and 2 in the range projection and σ_{new} is the new updated standard deviation for both units in the range projection (σ_y), as is seen also in Fig. 2.

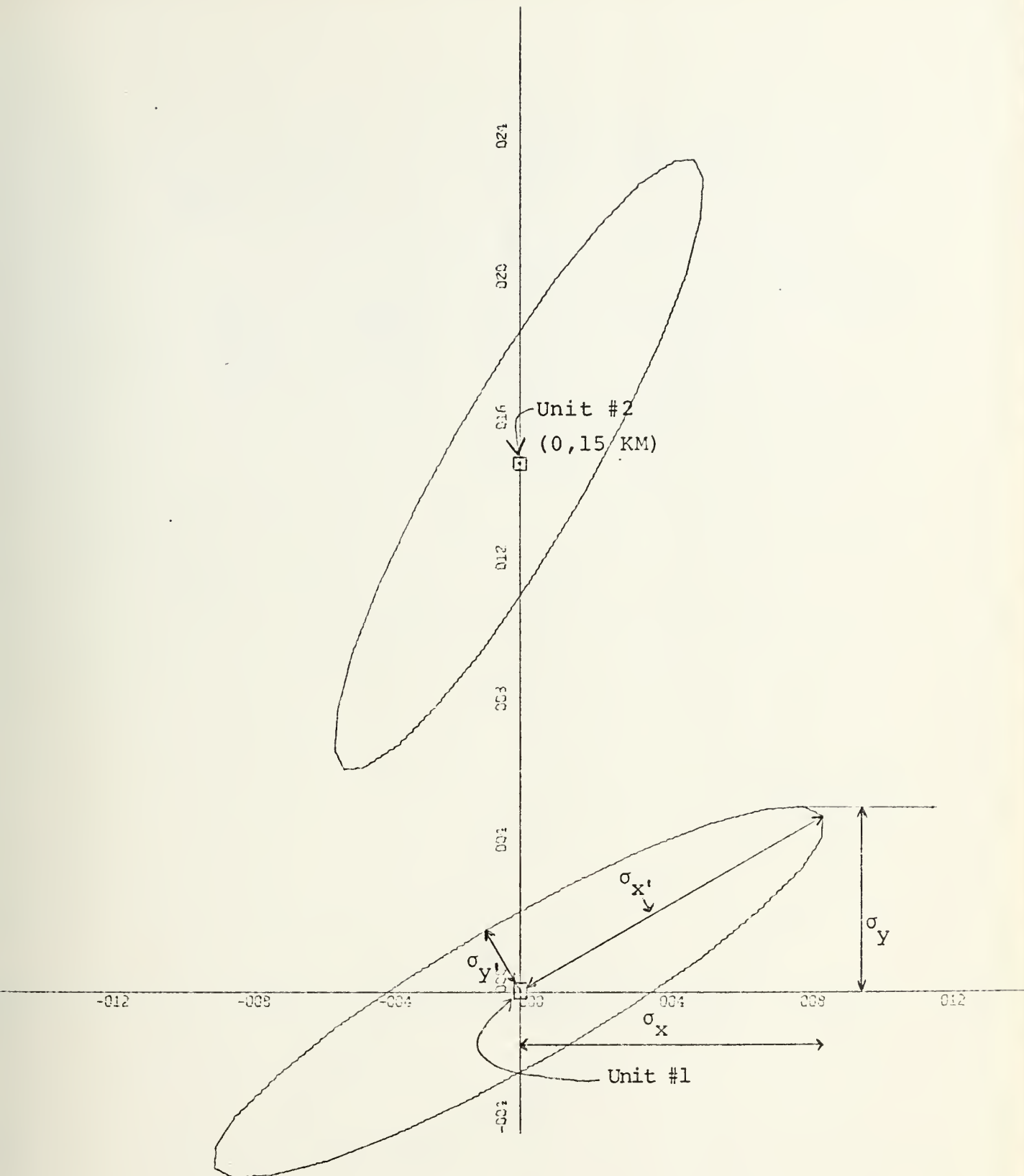


FIGURE 1. Error ellipsoids for two fixed units displaced along y-axis 15 KM

$$P_1 = \begin{bmatrix} 28 & 41.52 \\ 41.52 & 76 \end{bmatrix}$$

$$= \begin{bmatrix} \sigma_x^2 & \sigma_x \sigma_y \\ \sigma_x \sigma_y & \sigma_y^2 \end{bmatrix}$$

$$P_2 = \begin{bmatrix} 76 & 41.52 \\ 41.52 & 28 \end{bmatrix}$$

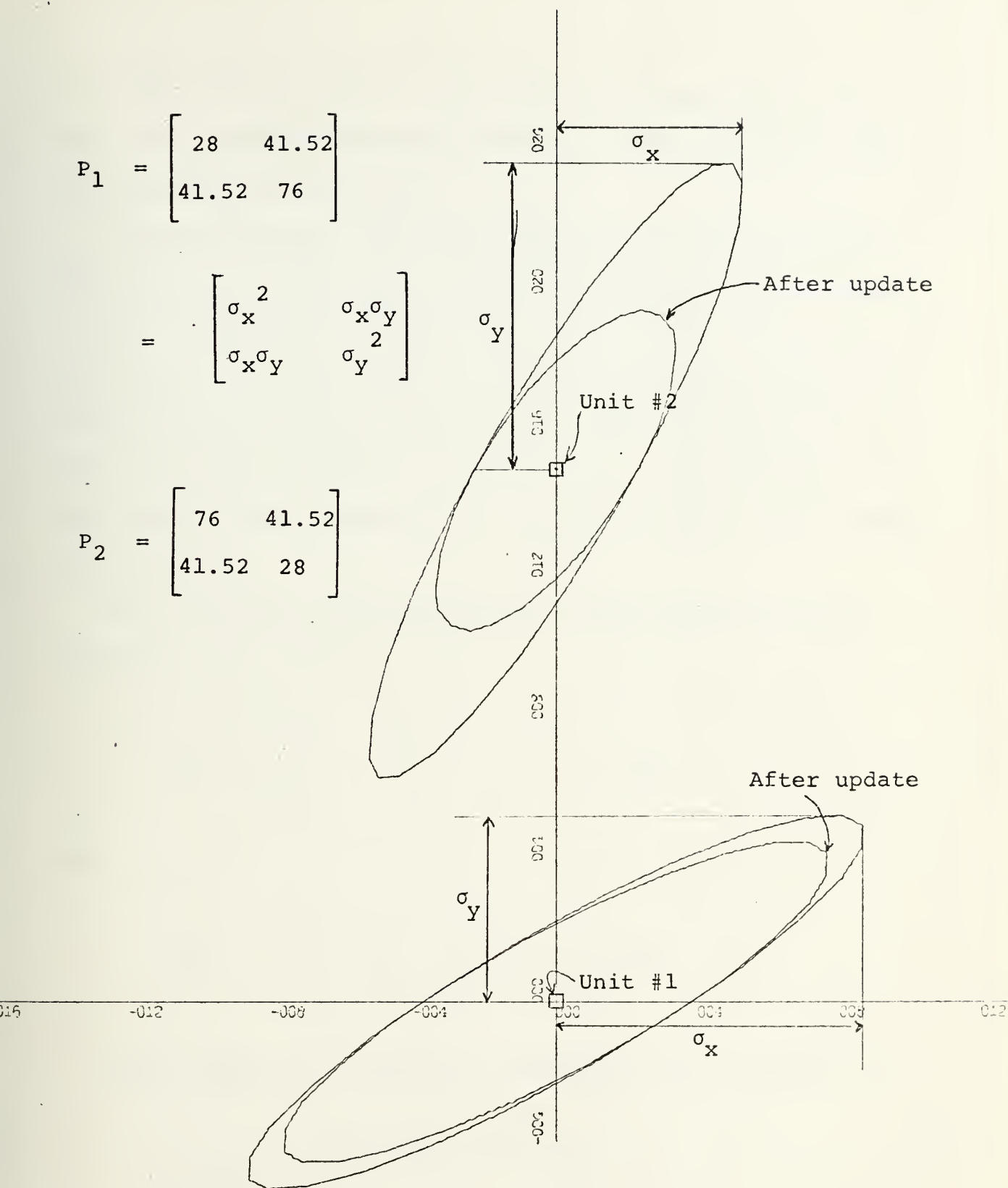


FIGURE 2. Projection of error ellipsoids to their x-y components and updated error ellipsoids after each unit ranges on the other

Thus the processing of an error free measurement between two units provides a better statistical description of both units along the range line.

This discussion considered fixed units with no velocity and only in the XY plane. Central to the equations employed in the Kalman filter are equations calculating the gains and the error covariance matrix. By merely adding the component of the variance of the ranging unit along the range line to the measurement noise in the calculation of the Kalman gains, the Kalman filter reduces the covariance matrix of the update unit properly.

The uncoupled error matrices and their directions are (from eqs. (22)-(24))

$$P_1' = \begin{bmatrix} 4 & 0 \\ 0 & 100 \end{bmatrix}, \quad \theta_1 = -30^\circ$$

and

$$P_2' = \begin{bmatrix} 100 & 0 \\ 0 & 4 \end{bmatrix}, \quad \theta_2 = +30^\circ$$

After update the resulting covariances are (see Fig. 2)

$$P_1(\text{new}) = \begin{bmatrix} 11.42 & 11.18 \\ 11.18 & 20.46 \end{bmatrix}$$

and

$$P_2(\text{new}) = \begin{bmatrix} 59.42 & 30.34 \\ 30.34 & 20.46 \end{bmatrix}$$

Their uncoupled equivalents

$$P_1'(\text{new}) = \begin{bmatrix} 3.89 & 0 \\ 0 & 28 \end{bmatrix}, \quad \theta_1(\text{new}) = -34^\circ$$

and

$$P_2'(\text{new}) = \begin{bmatrix} 7.6 & 0 \\ 0 & 3.89 \end{bmatrix}, \quad \theta_2(\text{new}) = 28.6^\circ$$

After ten updating operations

$$P_1(\text{new}) = \begin{bmatrix} 5.33 & 0.02 \\ 0.02 & 0.04 \end{bmatrix},$$

$$P_2'(\text{new}) = \begin{bmatrix} 14.52 & 0.06 \\ .06 & 0.04 \end{bmatrix}$$

and their uncoupled equivalents

$$P_1'(\text{new}) = \begin{bmatrix} 5.34 & 0 \\ 0 & .08 \end{bmatrix}, \quad \theta_1'(\text{new}) = 0.47^\circ$$

$$P_2' = \begin{bmatrix} 14.6 & 0 \\ 0 & .079 \end{bmatrix}, \quad \theta_2'(\text{new}) = 0.46^\circ$$

In Fig. 3 we see the influence of the sequential updating of the units, one upon the other over ten observations.

Note that the successive ranging in the y-direction effectively reduced the error variance in y and its projection in x due to the xy covariance. This was accomplished by assuming the measurement noise consists solely of the y component of the error variance of the other unit ranging upon it.

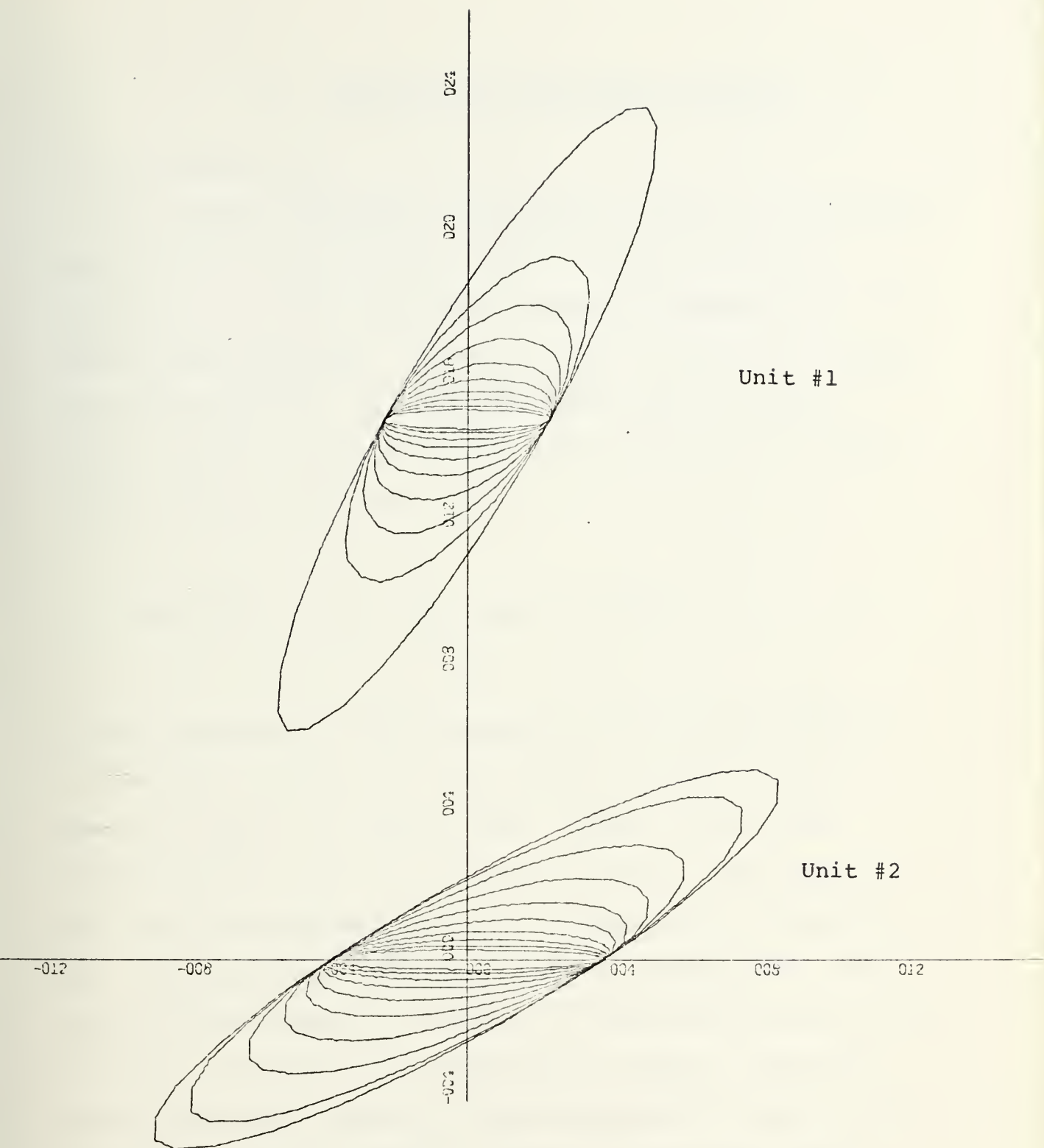


FIGURE 3. Sequential updating of the units, one upon the other, over ten observations

IV. TRACKING AND MANEUVERING TARGETS

A. THE CHOICE OF Q

One possible approach in designing a filter to accomodate maneuvers is to increase the random forcing excitation covariance, Q, until the filter adequately tracks the contemplated maneuvers. Normally this is done in a tracking simulation program. The running filter error residual, $(\underline{x}(k) - \hat{\underline{x}}(k/k))$ appears to be a better indicator of effectiveness than either mean error

$$\text{Mean Error} = \frac{1}{k} \sum_{j=1}^k (\underline{x}(j) - \hat{\underline{x}}(j/j))$$

or for that matter, error variance. Filter lag or bias as is best seen in the sign of the error, is lost in the squaring process for the variance. Also, the mean and variance error entail an accumulation of all error from start up to the present time. In a simulation, a maneuver may often not occur until well into a tracking run, and its effect may not appear as markedly in the mean error and error variance. A Monte Carlo simulation is often an effective design tool here. However, unless considerable engineering insight is used the resulting filter has been designed to handle the zero mean maneuver. That is, the filter will be designed against an ensemble of maneuvering tracks the mean of which is no maneuver at all. It appears that a more

successful procedure is to design against a highly probable worst case maneuver. The resulting filter should then be able to handle all possible contingencies, which is a necessary ingredient in most military systems.

The price paid in having a rather high Q in a filter design is an increased degradation in filter performance due to the measurement noise variance, R . In this application the measurement noise is minimal. The important thing is to attempt range measurements along the axis of maximum filter error variance as discussed in Section III.

B. SIMULATION RESULTS

An aircraft flying at Mach 1 follows a turn of radius 10 KM. Ranging unit 1 is located at the origin. Unit 2 is placed at (10 KM, 10 KM). We have the below filter parameters for Figs. 4 through 11 are

$$\Phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$$\Gamma = \begin{bmatrix} 0.5 & 0 \\ 1 & 0 \\ 0 & 0.5 \\ 0 & 1 \end{bmatrix}$$

and the initial conditions of

$$P(1/0) = \begin{bmatrix} 10^{-4} & 0 & 0 & 0 \\ 0 & 10^{-4} & 0 & 0 \\ 0 & 0 & 10^{-4} & 0 \\ 0 & 0 & 0 & 10^{-4} \end{bmatrix}$$

and

$$\underline{X}(1) = X(1/0) = \begin{bmatrix} 0 \\ 0.333 \text{ KM/S} \\ 10 \text{ KM} \\ 0 \end{bmatrix}$$

In Fig. 4 we have the first attempt at the algorithm for choosing the ranging unit nearest the line generated from the major axis of error in the error ellipsoid of the tracker. It ranged solely on unit 2 and failed to follow the turn. Similarly in Fig. 5, the filter ranged on unit 2 for the first half of the flight and on unit 1 for the second half.

The evolution of the design of the filter is presented here so that the errors in the design process may help to give insight into the filter's performance.

In Fig. 6 we see the beginning of proper functioning of the ranging algorithm (except on the last 20 observations). Note also that the covariance of excitation, Q , is insufficient to follow the maneuver as is indicated by the bias

in the filter track from the true track. Here we have

$$q_{11}/R = 2.5 \times 10^{-4}$$

from

$$R = 0.1$$

and

$$Q = \begin{bmatrix} .25 \times 10^{-4} & .5 \times 10^{-4} & 0 & 0 \\ .5 \times 10^{-4} & 1 \times 10^{-4} & 0 & 0 \\ 0 & 0 & .25 \times 10^{-4} & .5 \times 10^{-4} \\ 0 & 0 & .5 \times 10^{-4} & 1 \times 10^{-4} \end{bmatrix}$$

In Fig. 7 the algorithm appears to be functioning properly and there is sufficient Q for the filter to follow the turn. Here we have

$$q_{11}/R = 0.25$$

In Fig. 8 the filter was tested for its response to increasing the measurement noise (from $\sigma_v = 0.01$ KM to $\sigma_v = 0.1$ KM). It tracked well. However in Fig. 9, when the noise was again increased ($\sigma_v = 1$ KM) the track was lost immediately. This gives one a ball-park indication of filter performance as the ranging observations are degraded.

Figure 10 shows the filter performance with the error ellipsoids superimposed at every fifth observation. It indicates a short malfunction of the switching algorithm when the track crosses the x-axis. This was corrected in Fig. 11. The error ellipsoids are expanded to twenty-five times their true value in order that they may be seen.

In the appendix we have listed the computer simulation program with comments regarding its operation.

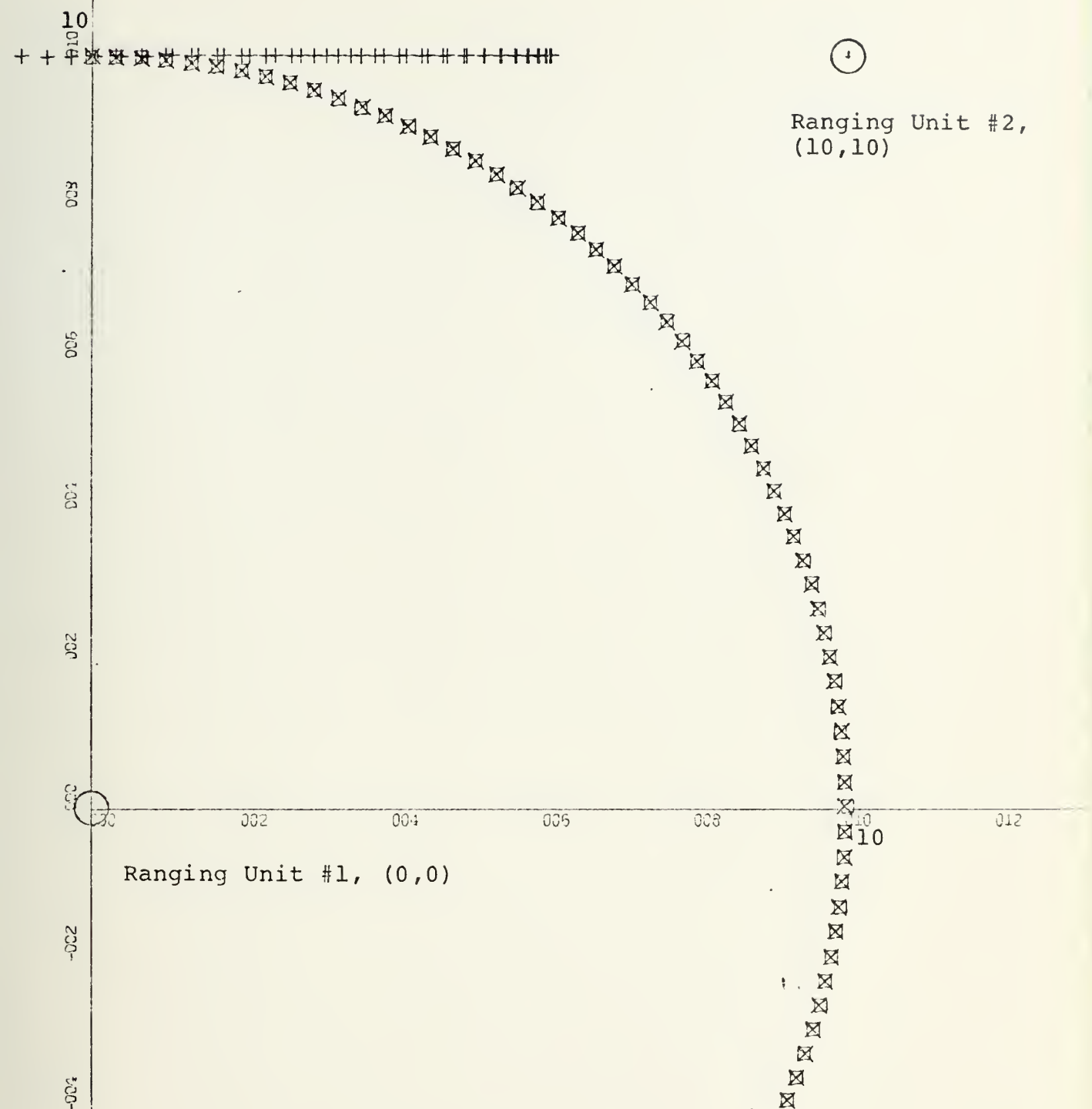


FIGURE 4. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging only on unit #2.
 x = true track, O = noise track, + = filter track

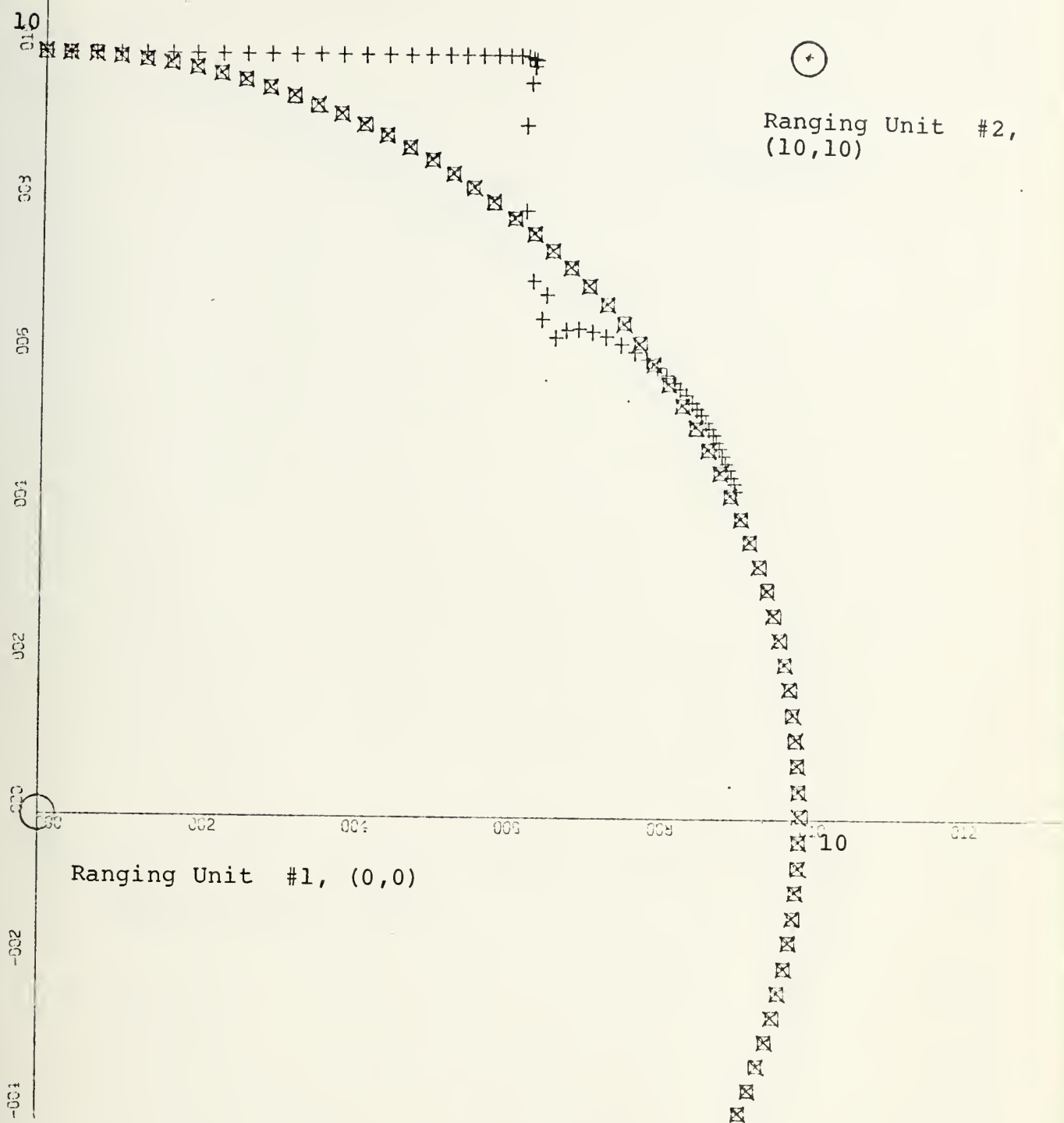


FIGURE 5. Aircraft in circular track at Mach 1 and radius 10 KM. Filter ranging on unit #2 and unit #1 during second half.
 x = true track, o = noise track, + = filter track

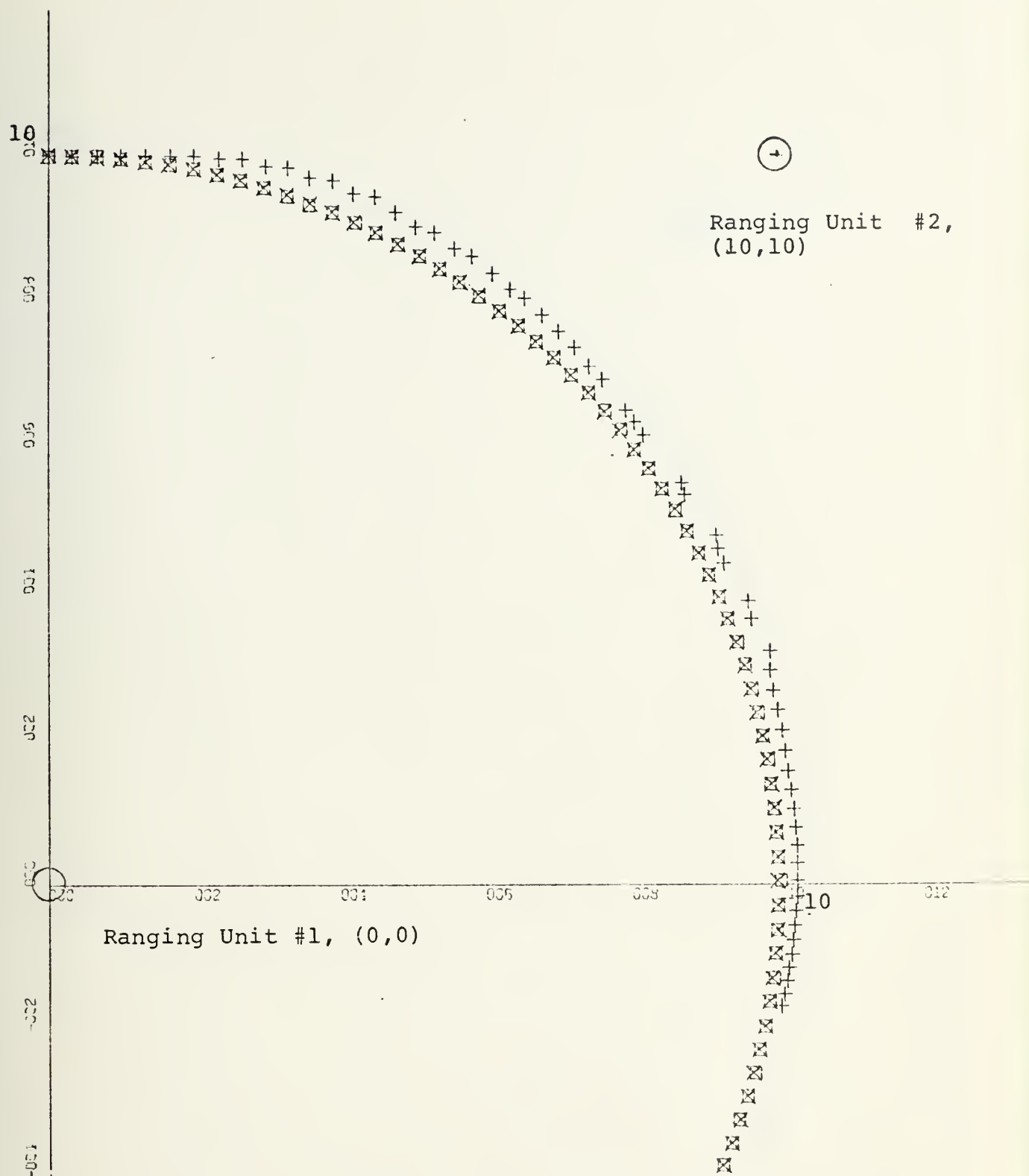


FIGURE 6. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working poorly in last third of flight (unit #1 ranges solely on last 20 observations. A too low Q is indicated by the track bias.
 x = true track, o = noise track, + = filter track

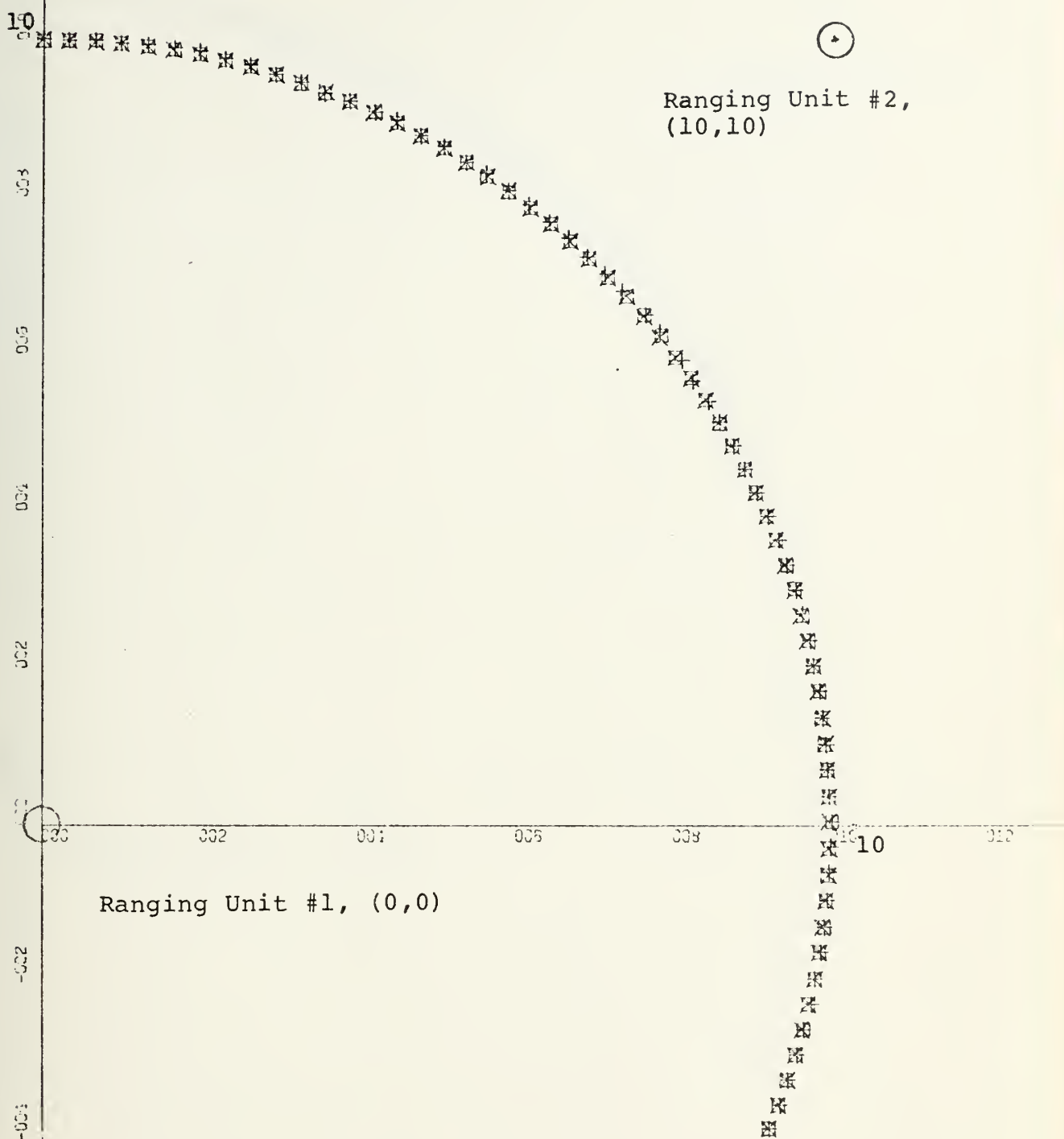


FIGURE 7. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 10 M.
x = true track, o = noise track, + = filter track

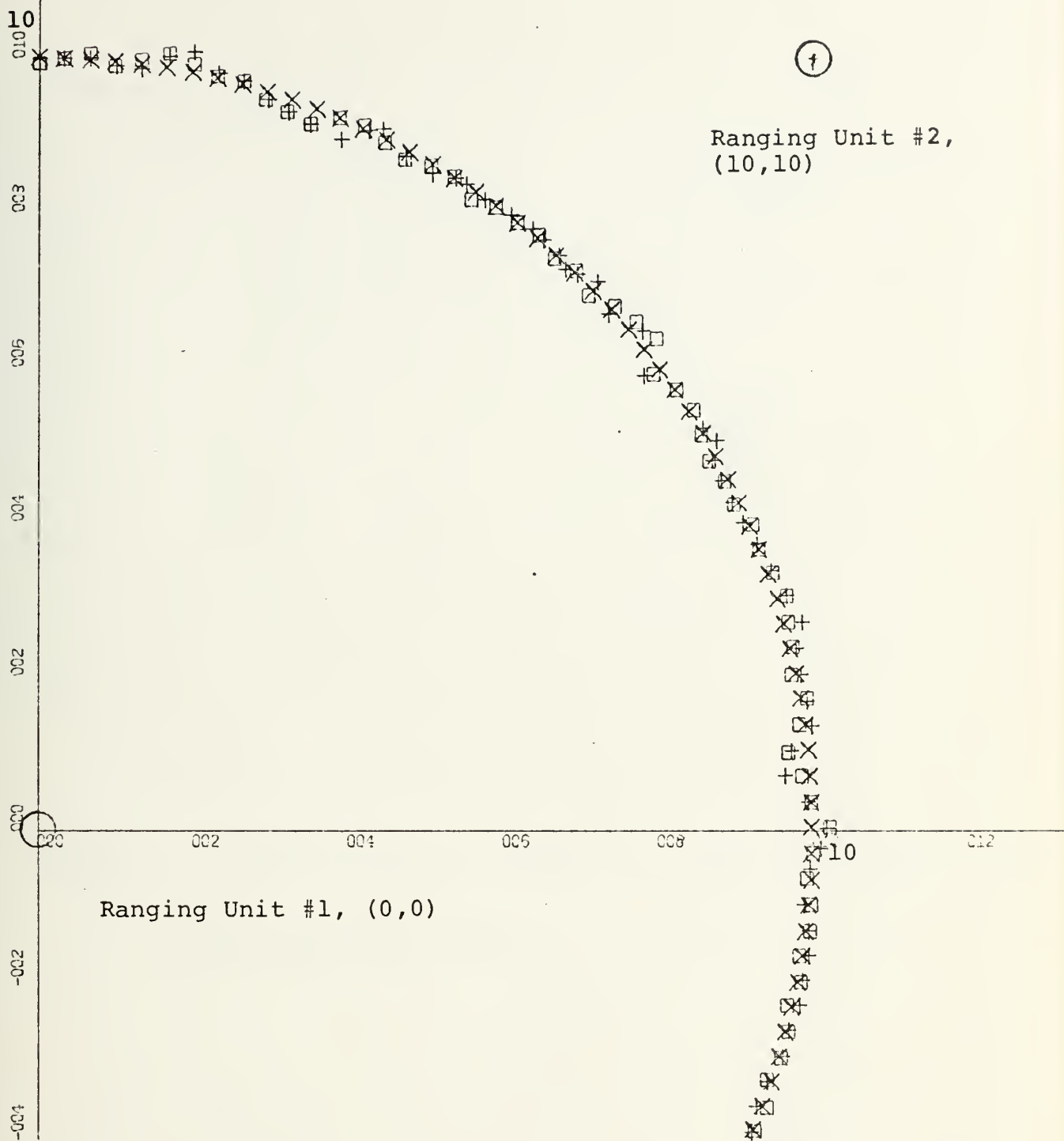


FIGURE 8. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Measurement noise = 100 M.
 x = true track, o = noise track, + = filter track



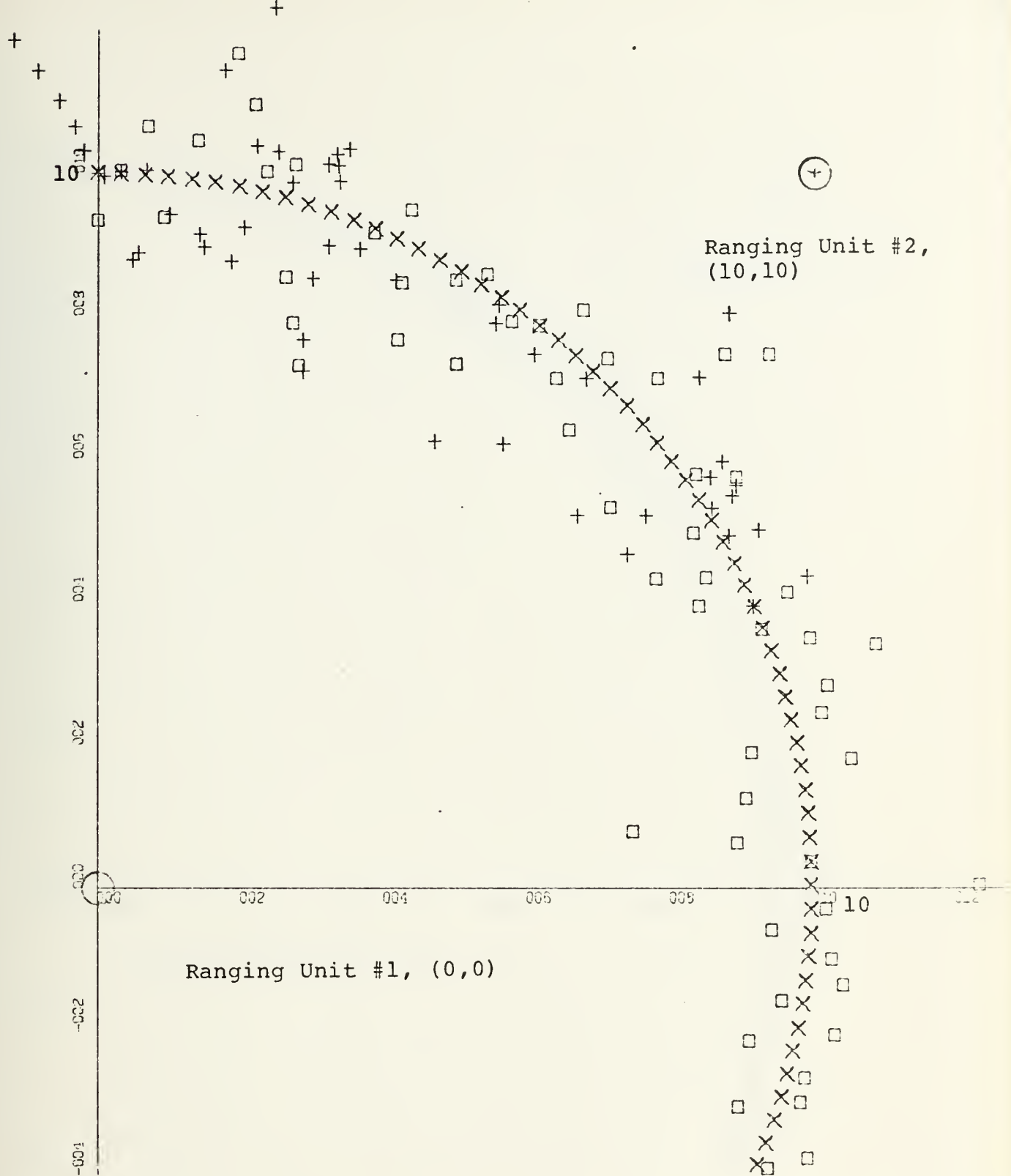


FIGURE 9. Aircraft in circular track at Mach 1 and radius 10 KM. Algorithm for choosing which ranging unit working. Q sufficient to allow filter to adequately track the turning maneuver. Filter drops track. Measurement noise = 1 KM. x = true track, o = noise track, $+$ = filter track



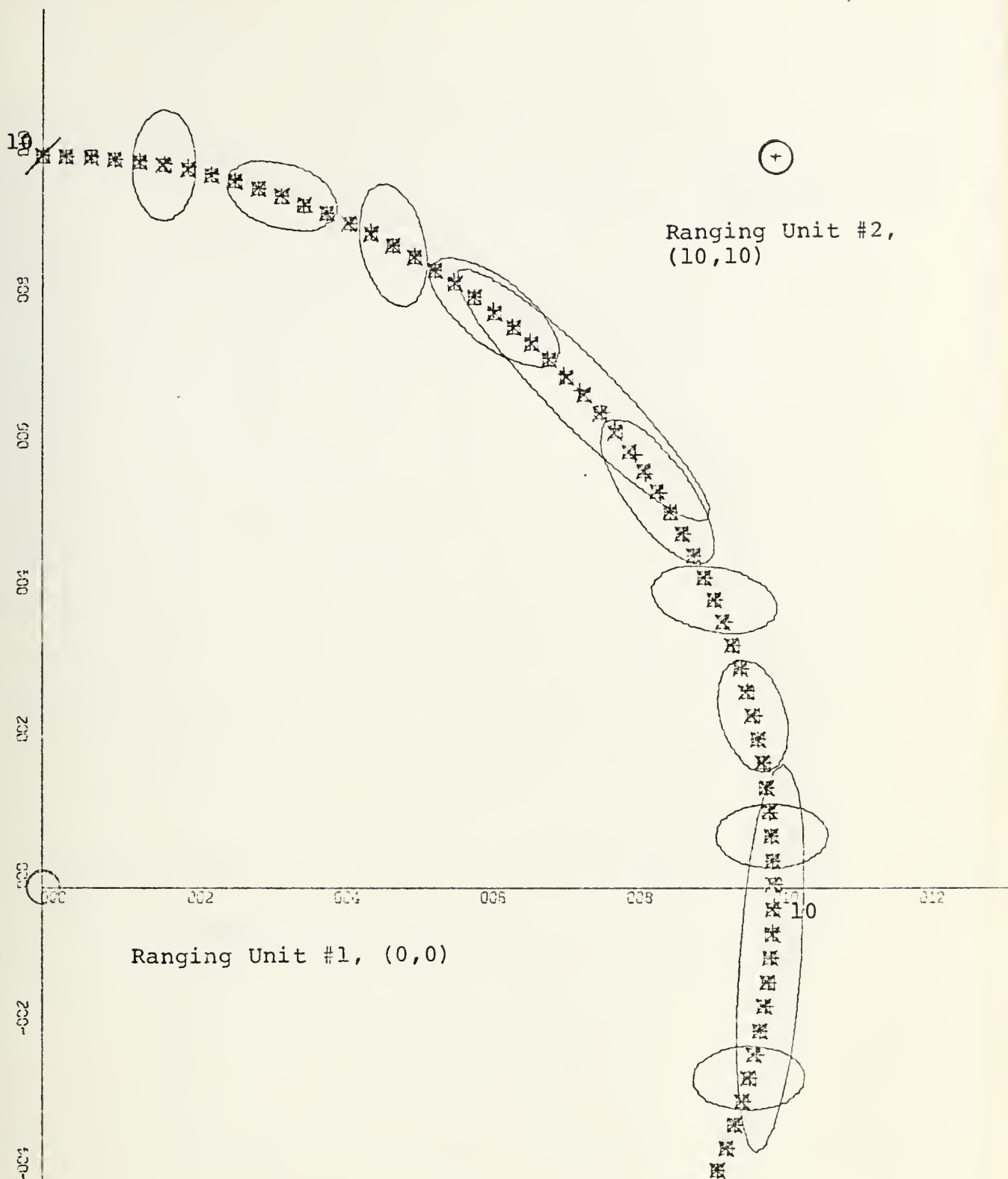


FIGURE 10. Aircraft in circular track at Mach 1 and radius of 10 KM. Error ellipsoids presented on every fifth observation. Measurement noise = 10 M. Switching algorithm fails on x-axis. Ellipses 25 times true scale.
 x = true track, o = noise track, + = filter track



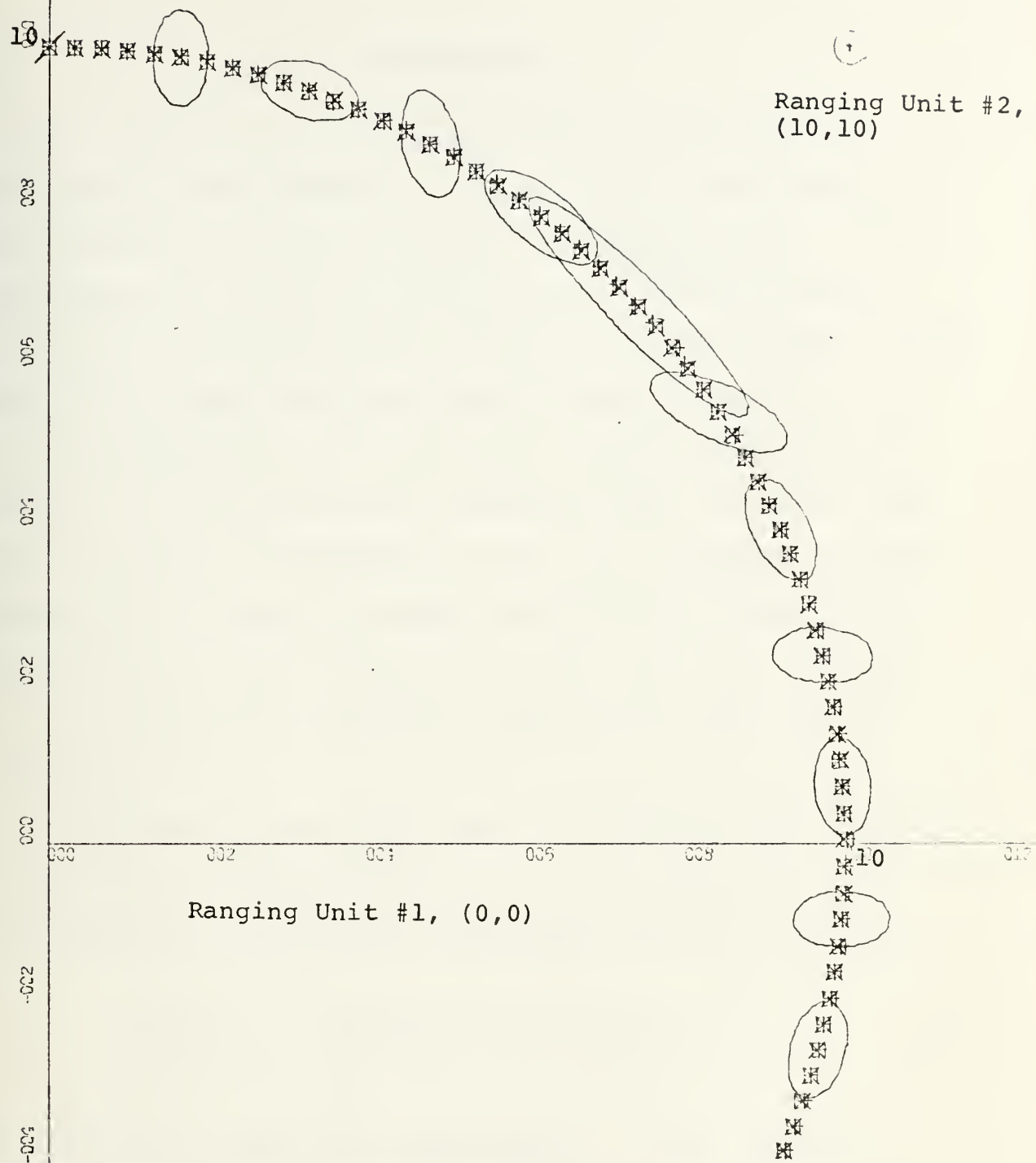


FIGURE 11. Aircraft in circular track at Mach 1 and radius of 10 KM. Switching algorithm corrected. Ellipses 20 times true scale. x = true track, o = noise track, + = filter track



V. CONCLUSIONS

The evolution of this filter design appears to have some merit. The maneuvering target can be tracked handily with adequate choice of Q . The filter operated well in all but impossible ranging noise situations. The real system has range noise on the order of ten meters. The filter tracked well with a range noise sigma of one hundred meters.

The algorithm for choosing which unit to link to for ranging is finally operating satisfactorily. In fact, this may be the real contribution of this work. Another possible benefit is the use of graphical presentation of the error ellipsoids in filter evaluation. They were most essential in the algorithm for choosing ranging links and in the Q evaluation.

Still to be accomplished are: an initialization algorithm, a spurious data gating scheme and a track deletion logic. The latter two items may be dispatched readily by letting

$$\text{Gate}(k) = 3 \sqrt{P_{11}(k/k-1) + R_{11}(k)}$$

and if a unit receives no range update. Within the gate for, say, six update sequence times, then reinitialize and start over.

The rotation and reduction of the error ellipsoids (i.e. the filter error covariance) was most instructive and gave much insight into the performance of the filter.

FILTER FOR STATIC UNITS TRACKING

```
// EXEC FORTCLGP, REGION.GO=150K
//FORT.SYSIN DD *
REAL*4LA(8)/ 'G11 ','G12 ','G22 ','G42 ','PK11','PK22','PK33',
* ,PK44,/
DIMENSION HI(12,12),Q(12,12),H(12,12),R(12,12),G(12,12),
&PHIT(12,12),PHI(12,12),XY(800),
&G22(800),PKK(12,12),PKKM1(12,12),G11(800)
DIMENSION PINV(12,12)
DIMENSION IREAD(10),IWRITE(10)
DIMENSION DEL(12,12),A(12,12),B(12,12),D1(12,12),D2(12,12)
DIMENSION AA(12,12),YY(12),Z(12)
DIMENSION DELT(12,12)
DIMENSION G21(800)
DIMENSION G31(800),G42(800)
DIMENSION C(12,12),D(12,12),DD(12,12)
DIMENSION XP(50),YP(60)
INTEGER*4 ITB(12)/12*0/
REAL*4 RTB(28)/28*0.0/
EQUIVALENCE (ITITLE,RTB(5))
REAL*8 ITITLE(12)/'X' = TRUE, + = FILTER, SQUARE = NOISY'/
```

THIS PROGRAM COMPUTES THE FOLLOWING KALMAN FILTER EQUATIONS

$$G(K) = P(K/K-1) * HT * (H * P(K/K-1) * HT + R)^{-1}$$

$$P(K/K) = (I - G(K) * H) * P(K/K-1)$$

$$P(K/K-1) = PHI * P(K-1/K-1) * PHIT + Q$$

Q(I,J) DEFINES THE COVARIANCE OF THE PER SAMPLE RANDOM GAUSSIAN EXCITATION OF THE PROCESS.

R(I,J) DEFINES THE RANDOM (GAUSSIAN) MEASUREMENT NOISE COVARIANCE WHICH IS ADDED TO THE OBSERVABLE SIGNALS.

HI(I,J) IS THE IDENTITY MATRIX.

II=K(THE DISCRETE POINT IN TIME-THE STAGE OF THE PROCESS)

PKK(I,J) = P(K/K), (COV ERROR AT K GIVEN K SAMPLES)

PKKM1(I,J)=P(K/K-1), (COV ERROR AT K GIVEN K-1 SAMPLES)

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC


```

C  N= NUMBER OF ROWS,      M= NO. OF COL... OBS..., ND AND MD ARE THE DIMENSIONS
C  NN=NUMBER OF ITERATIONS OF FILTER
      LD=12
      READ(5,50)N,M,ND,MD,LD,NN,DT,IWRITE,IWRITE
50  FORMAT(6I5,1F10.4/10A4,10A4)
      WRITE(6,7777)
7777 FORMAT(1H1)
      WRITE(6,51)N,M,ND,MD,LD,NN,DT
51  FORMAT(2X,2HN=,I5,5X,2HM=,I5,5X,3HND=,I5,5X,3HMD=,I5,5X,3HLD=,
1  I5,5X,3HNN=,I5,3HDT=,F10.4)
      CALL MREAD(R,N,N,ND,MD,IWRITE)
      WRITE(6,53)
53  FORMAT(/12H MATRIX R /)
      CALL MWRITE(R,N,N,ND,MD,IWRITE)
      CALL MREAD(Q,N,N,ND,MD,IWRITE)
      WRITE(6,54)
      CALL MWRITE(Q,N,N,ND,MD,IWRITE)
54  FORMAT(/12H MATRIX Q /)
      CALL MREAD(PKKM1,N,N,ND,MD,IWRITE)
      WRITE(6,55)
55  FORMAT(/13H MATRIX PKKM1 /)
      CALL MWRITE(PKKM1,N,N,ND,MD,IWRITE)
      XDOT2(0)=V*57.3*DT(SEC)/R#3600
      CALL MREAD(PHI,N,N,ND,MD,IWRITE)
      CALL PHIDEL(DT,N,M,A,B,PHI,DEL,D1,D2,ND,MD,LD)
58  FORMAT(/13H MATRIX PHI /)
      WRITE(6,58)
      CALL MWRITE(PHI,N,N,ND,MD,IWRITE)
      CALL MREAD(H,N,N,ND,MD,IWRITE)
      WRITE(6,59)
59  FORMAT(/13H MATRIX H /)
      CALL MWRITE(H,N,N,ND,MD,IWRITE)
      CALL MREAD(HI,N,N,ND,MD,IWRITE)
      WRITE(6,60)
60  FORMAT(/13H MATRIX HI /)
      CALL MWRITE(HI,N,N,ND,MD,IWRITE)
      CALL PROD(HI,HI,N,N,N,D,ND,MD,LD)
      WRITE(6,7777)
      T=0.0
      L=1
      ST=0.0
      MN=0
      CLOCK=ITIME(0)*0.01
      WRITE(6,52)
52  FORMAT(/12H MATRIX G /)
      ITB(1)=1
      ITB(8)=2
      ITB(9)=1

```



```

1  ITB(10)=2
   ITB(11)=4
   RTB(1)=4
   RTB(2)=4
   DO 100 I=1,NN
      THE1=0.5*ATAN(2.*PKKM1(1,2)/(PKKM1(1,1)-PKKM1(2,2)))
      THE2=0.5*ATAN(2.*PKKM1(3,4)/(PKKM1(3,3)-PKKM1(4,4)))
      SIG2X=(PKKM1(1,1)+PKKM1(2,2))/2.+PKKM1(1,2)/SIN(2.*THE1)
      SIG2Y=(PKKM1(1,1)+PKKM1(2,2))/2.-PKKM1(1,2)/SIN(2.*THE1)
      SIG2X2=(PKKM1(3,3)+PKKM1(4,4))/2.+PKKM1(3,4)/SIN(2.*THE2)
      SIG2Y2=(PKKM1(3,3)+PKKM1(4,4))/2.-PKKM1(3,4)/SIN(2.*THE2)
      SX=(SIG2X)**.5
      SY=(SIG2Y)**.5
      PT=3.14159265/12.
      CT=COS( THE1 )
      ST=SIN( THE1 )
      DO 1 I=1,25
         XI=I
         XP(I)=SX*COS( PT*XI)*CT-SY*SIN(PT*XI)*ST
         YP(I)=SX*COS( PT*XI)*ST+SY*SIN(PT*XI)*CT+ 15.
         CALL DRAWP(25,XP,YP,ITB,RTB)
         SX=(SIG2X2)**.5
         SY=(SIG2Y2)**.5
         CT=COS( THE2 )
         ST=SIN( THE2 )
         DO 7 I=1,25
            XI=I
            XP(I)=SX*COS( PT*XI)*CT-SY*SIN(PT*XI)*ST
            YP(I)=SX*COS( PT*XI)*ST+SY*SIN(PT*XI)*CT
            IF(II.LT.NN) GO TO 2
            ITB(I)=3
            CONTINUE
            CALL DRAWP(25,XP,YP,ITB,RTB)
            DERAD=360./((3.14159265*2.))
            THE1=DERAD*THE1
            THE2=DERAD*THE2
            WRITE (6,146) THE1,SIG2X,SIG2Y,THE2,SIG2X2,SIG2Y2
            FORMAT (9(2X,1PE12.5),/)
            R(1,1)=PKKM1(4,4)
            R(2,2)=PKKM1(2,2)
            CALL GA IN(PKK,PKKM1,Q,R,PHI,H,N,M,G,HI,ND,MD,LD)
            ST=I/1
            IF(T-ST) 20,20,21
            MM=MM+1
            G11(NM)=G(1,1)
            G12(NM)=G(1,2)
            G21(NM)=G(2,1)

```



```

G22(MM)=G(2,2)
XY(MM)=MM-1
WRITE(6,5)I
5 FORMAT(/20X,5HTIME=,I5)
C CALL PROD(HI,PKKM1,N,N,N,D1,ND,MD,LD)
C NOTE THAT THIS RECIPI SR DESTROYS THE INPUT MATRIX
C CALL RECIPI(N,0.000001,C1,PINV,KER,MD)
C CALL TRANS(PHI,N,N,PHIT,ND,ND)
C CALL PROD(PKK,PHIT,N,N,N,A,ND,MD,LD)
C CALL PROD(A,PINV,N,N,C,ND,MD,LD)
C CALL PROD(D,C,N,N,N,DD,ND,MD,LD)
C CALL PROD(DD,HI,N,N,N,D,ND,MD,LD)
C WRITE(6,557)
557 FORMAT(/13H MATRIX D )
C CALL MWRITE(C,N,N,ND,MD,IWRITE)
C CALL MWRITE(A,N,N,ND,MD,IWRITE)
C CALL MWRITE(D,N,N,ND,MD,IWRITE)
C WRITE(6,555)
555 FORMAT(/13H MATRIX PKK )
C CALL MWRITE(PKK,N,N,ND,MD,IWRITE)
C WRITE(6,55)
C CALL MWRITE(PKKM1,N,N,ND,MD,IWRITE)
C WRITE(6,556)
556 FORMAT(/13H MATRIX PINV )
C CALL MWRITE(PINV,N,N,ND,MD,IWRITE)
C WRITE(6,99)
99 FORMAT(/13H MATRIX G /)
21 CALL MWRITE(G,N,N,ND,MD,IWRITE)
C CONTINUE
I=I+DT
1000 CONTINUE
MC=0
CALL SSPLOT(XY,G11,MM,MC,TITLE,0,XMIN,XMAX,YMIN,YMAX)
CALL SSPLOT(XY,G21,MM,MC,TITLE,0,XMIN,XMAX,YMIN,YMAX)
END
SUBROUTINE SSPLOT(X,Y,N,MC,TITLE,ISC,XMIN,XMAX,YMIN,YMAX)
DIMENSION X(1),Y(1),GRID(33,81),XS(9),YS(9),TITLE(16)
INTEGER*4 GRID,BLANK/' ',DOT/'.',PLUS/'+',XCHAR(4)/'+','*','.',#',
*,&/'
* IF(MC-1)1,1,15
1 NC=4
IF(ISC)13,13,14
13 XMAX=-1.0E+20
XMIN=-XMAX
YMAX=XMAX
YMIN=-XMAX
DO 11 I=1,N
IF(X(I)-XMAX)3,3,2

```



```

2  XMAX=X(I)
3  YXMAX=Y(I)
4  IF(X(I)-XMIN)4,4,5
5  XMIN=X(I)
6  YXMIN=Y(I)
7  IF(Y(I)-YMAX)7,7,6
8  YMAX=Y(I)
9  XYMAX=X(I)
10 IF(Y(I)-YMIN)8,8,11
11 YMIN=Y(I)
12 XYMIN=X(I)
13 CONTINUE
14 IERR=0
15 IF(MC-1)32,32,21
21 NC=NC+4
22 DO 31 I=1,N
23 IF(X(I)-XMAX)23,23,22
24 X(I)=XMAX
25 IERR=IERR+1
26 GO TO 25
27 IF(X(I)-XMIN)24,25,25
28 X(I)=XMIN
29 IERR=IERR+1
30 IF(Y(I)-YMAX)27,27,26
31 Y(I)=YMAX
32 IERR=IERR+1
33 GO TO 31
34 IF(Y(I)-YMIN)28,31,31
35 Y(I)=YMIN
36 IERR=IERR+1
37 CONTINUE
38 IF(MC-2)33,71,71
39 XR=XMAX-XMIN
40 YR=YMAX-YMIN
41 DO 41 K=1,81
42 DO 41 I=1,33
43 GRID(I,K)=BLANK
44 XTEST=XMAX*XMIN
45 YTEST=YMAX*YMIN
51 IF(XTEST)51,51,61
52 IYAXIS=80.0*(-XMIN)/XR+1.5
53 DO 52 I=1,33
54 GRID(I,IYAXIS)=DOT
61 IF(YTEST)62,62,71
62 IXAXIS=32.0*YMAX/YR+1.5
63 DO 63 J=1,81
64 GRID(IXAXIS,J)=DOT
71 CONTINUE

```



```

72 IF(MC-1)72,72,73
73 JSET=0
74 JSET=JSET+1
75 IF(JSET-4)75,74,74
81 JSET=1
82 DO 91 I=1,N
83 IPTX=32.0*(YMAX-Y(I))/YR+1.5
84 IPTY=80.0*(X(I)-XMIN)/XR+1.5
89 IF(IPTX-33)81,81,89
91 IF(IPTX-81)82,82,89
101 IF(IPTX)89,89,83
102 IF(IPTY)89,89,84
103 GRID(IPTY,IPTX)=XCHAR(JSET)
111 GO TO 91
121 IERR=IERR+1
122 CONTINUE
131 IF(MC-1)111,111,101
151 IF(MC-2)103,102,103
161 RETURN
162 GO TO 151
163 XINCR=XR/8.0
164 YINCR=YR/8.0
165 XS(1)=XMIN
166 YS(1)=YMAX
167 DO 121 I=2,9
168 XS(I)=XS(I-1)+XINCR
169 YS(I)=YS(I-1)-YINCR
170 IF(MC-1)151,102,131
171 IF(MC-2)102,102,151
172 PRINT 80
173 PRINT 10,(XS(I),I=1,9)
174 II=1
175 I=0
176 DO 201 IK=1,33
177 IF(I)161,161,162
178 PRINT 20,YS(II),(GRID(IK,IX),IX=1,81),YS(II)
179 II=II+1
180 GO TO 165
181 PRINT 30,(GRID(IK,IX),IX=1,81)
182 I=I+1
183 IF(I-4)201,171,171
184 I=0
185 CONTINUE
186 PRINT 40,(XS(I),I=1,9)
187 PRINT 90,(TITLE(I),I=1,NC)
188 IF(IERR)211,211,202
189 PRINT 50,IERR
202

```



```

211 IF(ISC)212,212,102
212 PRINT 60,YMAX,XYMAX,YMIN,XYMIN
PRINT 70,XMAX,YXMAX,XMIN,YXMIN
RETURN
10 FORMAT(11X,1PE9.2,8(1X,E9.2)/13X,2H**,8(10H+*****),3H+**)
20 FORMAT(1X,1PE10.3,2X,1H+,1X,81A1,1X,1H+2X,E10.3)
30 FORMAT(13X,1H*,1X,81A1,1X,1H*)
40 FORMAT(13X,2H**,8(10H+*****),3H+**/11X,1PE9.2,8(1X,E9.2))
50 FORMAT(1X,NUMBER OF POINTS OUT OF RANGE=,I4)
60 FORMAT(1X,MAX Y=,1PE12.4,AT X=,E12.4,10X,MIN Y=,E12.4,AT X=
*,E12.4)
70 FORMAT(1X,MAX X=,1PE12.4,AT Y=,E12.4,10X,MIN X=,E12.4,AT Y=
*,E12.4)
80 FORMAT(1H1)
90 FORMAT(1X,4A4,4H=+,4A4,4H=*,4A4,4H=#,4A4,4H=E)
END
SUBROUTINE PHIDEL(T,N,M,A,B,PHI,DEL,D1,D2,ND,MD,LD)
DIMENSION A(12,12),B(12,12),PHI(12,12),DEL(12,12),TERM(12,12),
1COR(12,12),C(12,12),D1(12,12),D2(12,12),TEIL(12,12)
TEST=1.E-7
F=1.
DO 10 IR=1,N
DO 10 IC=1,N
PHI(IR,IC)=0.
PHI(IR,IR)=1.
C(IR,IC)=A(IR,IC)
TEIL(IR,IC)=T/2.00*PHI(IR,IC)
TERM(IR,IC)=T*PHI(IR,IC)
DO 11 IR=1,N
DO 11 IC=1,N
COR(IR,IC)=T/F*C(IR,IC)
PHI(IR,IC)=PHI(IR,IC)+COR(IR,IC)
TEIL(IR,IC)=TEIL(IR,IC)+T/(F+1.
)*COR(IR,IC)
TERM(IR,IC)=TERM(IR,IC)+T/(F+1.
)*COR(IR,IC)
DO 12 IR=1,N
DO 12 IC=1,N
C(IR,IC)=0.
DO 12 K=1,N
C(CR,IC)=C(IR,IC)+A(IR,K)*COR(K,IC)
F=F+1.
DO 13 IR=1,N
DO 13 IC=1,N
IF(ABS(COR(IR,IC)).GT.TEST*ABS(PHI(IR,IC))) GO TO 50
13 CONTINUE
CALL PROD(TERM,B,N,N,M,DEL,ND,MD,LD)
CALL PROD(TEIL,B,N,N,M,D2,ND,MD,LD)
DO 14 IR=1,N
DO 14 IC=1,M

```



```

14 D1(IR,IC)=DEL(IR,IC)-D2(IR,IC)
RETURN
END
C THIS SUBROUTINE COMPUTES THE OPTIMUM GAIN MATRIX AND THE ERROR
C COVARIANCE
SUBROUTINE GAIN(PKK,PKKM1,Q,R,PHI,H,N,M,G,HI,ND,MD,LD)
ODIMENSION PKK(12,12),Q(12,12),HI(12,12),HT(12,12)
1 G(12,12),R(12,12),PHI(12,12),PHIT(12,12),TEMP(12,12),TEMP2(12,12)
2 TEMPI(12,12)=P(K/K-1)*HI*(H*(K/K-1)*HT + R)
G(K) = P(K/K-1)*HI*(H*(K/K-1)*HT + R)
CALL TRANS(H,N,N,HT,ND,MD)
CALL PROD(PKKM1,HT,N,N,TEMP,ND,MD,LD)
CALL PROD(H,TEMP,N,N,TEMPI,ND,MD,LD)
CALL ADD(TEMPI,R,N,N,TEMPI,ND,MD)
CALL RECIP(M,0.000001,TEMPI,TEMP2,KER,MD)
IF (KER-2) 101,110,101
110 WRITE(6,111)
111 FORMAT(5HKER=2)
101 CALL PROD(TEMP,TEMP2,N,N,G,ND,MD,LD)
C NOTE HERE PKK(I,J) = P(K/K) WHERE
C P(K/K) = (I-G(K)*H)*P(K/K-1)
CALL PROD(G,H,N,N,TEMP,ND,MD,LD)
DO 108 I=1,N
DO 108 J=1,N
TEMP(I,J)=TEMP(I,J)
CALL ADD(HI,TEMP,N,N,TEMP,ND,MD)
CALL PROD(TEMP,PKKM1,N,N,P(K/K-1),ND,MD,LD)
C NOTE HERE PKKM1(I,J) = P(K/K-1) WHERE
C P(K/K-1) = PHI*P(K-1/K-1)*PHIT + Q
CALL TRANS(PHI,N,N,PHIT,ND,MD)
CALL PROD(PKK,PHIT,N,N,TEMP,ND,MD,LD)
CALL PROD(PHI,TEMP,N,N,TEMPI,ND,MD,LD)
CALL ADD(TEMPI,Q,N,N,PKKM1,ND,MD)
RETURN
END
SUBROUTINE ADD (A,B,N,M,C,ND,MD)
DIMENSION A(ND,MD),B(ND,MD),C(ND,MD)
DO 152 I=1,N
DO 152 J=1,M
C(I,J) = A(I,J) + B(I,J)
152 RETURN
END
SUBROUTINE SUB (A,B,N,M,C,ND,MD)
DIMENSION A(ND,MD),B(ND,MD),C(ND,MD)
DO 152 I=1,N
DO 152 J=1,M
C(I,J) = A(I,J) - B(I,J)
152 RETURN

```

01
02
03
04
05
5A
06
07
08
09
10
11


```

END
SUBROUTINE PROD (A,B,N,M,L,C,ND,MD,LD)
DIMENSION A(ND,MD),B(MD,LD),C(ND,LD)
DO 1 I=1,ND
DO 1 J=1,LD
1 C(I,J)=0.
DO 151 I=1,N
DO 151 J=1,L
DO 151 K=1,M
151 C(I,J) = C(I,J) + A(I,K)*B(K,J)
RETURN
END
SUBROUTINE TRANS(A,N,M,C,ND,MD)
DIMENSION A(ND,MD),C(MD,ND)
DO 153 I=1,N
DO 153 J=1,M
153 C(J,I) = A(I,J)
RETURN
END
SUBROUTINE CONST(Q,A,N,M,C,ND,MD)
DIMENSION A(ND,MD),C(ND,MD)
IF(Q)11,10,11
10 DO 100 I=1,N
DO 100 J=1,M
100 C(I,J) = 0.0
RETURN
11 IF(Q-1.0)13,12,13
12 DO 120 I=1,N
DO 120 J=1,M
120 C(I,J) = A(I,J)
RETURN
13 IF(Q+1.0)15,14,15
14 DO 140 I=1,N
DO 140 J=1,M
140 C(I,J) = -A(I,J)
RETURN
15 DO 150 I=1,N
DO 150 J=1,M
150 C(I,J) = Q*A(I,J)
RETURN
END
SUBROUTINE RECIP(N,EP,B,X,KER,M)
DIMENSION A(12,12),X(M,M),B(M,M)
CALL CONST(1.,B,N,N,A,12,12)
DO 1 J=1,M
DO 1 I=1,M
1 X(I,J)=0.
DO 2 K=1,N

```

```

12
13
14
14A
14B
14C
15
16
18
19
19A
20
21
22
23
24
25
26
27
28
30
31
32
33
35
36
37
38
40
41
42
43
44
45
46
47
000040
000050

```


000060
000070
000080
000090
000100

000130
000140
000160
000170
000180
000190
000200
000210
000220
000230

000260
000270

000290
000300
000310
000320
000330
000340
000350
000360
000370
000380
000390

000410

000430
000440
000450
000460
000470

000480

```

2  X(K,K)=1.
10 DO 34 L=I,N
   KP=0
   Z=0.
   DO 12 K=L,N
     IF(Z.GE.ABS(A(K,L))) GO TO 12
     Z=ABS(A(K,L))
11  KP=K
12  CONTINUE
13  IF(L.GE.KP) GO TO 20
   DO 14 J=L,N
     Z=A(L,J)
     A(L,J)=A(KP,J)
     A(KP,J)=Z
14  A(KP,J)=Z
   DO 15 J=1,N
     Z=X(L,J)
     X(L,J)=X(KP,J)
     X(KP,J)=Z
15  X(KP,J)=Z
20  IF(ABS(A(L,L)).LE.EP) GO TO 50
30  IF(L.GE.N) GO TO 34
31  LPI=L+1
   DO 36 K=LPI,N
     IF(A(K,L).EQ.0.) GO TO 36
     RATIO=A(K,L)/A(L,L)
     DO 33 J=LPI,N
       A(K,J)=A(K,J)-RATIO*A(L,J)
     DO 35 J=1,N
       X(K,J)=X(K,J)-RATIO*X(L,J)
36  CONTINUE
34  DO 43 I=1,N
   I1=N+1-I
   DO 43 J=1,N
     S=0.
     IF(I1.GE.N) GO TO 43
     IIP1=I1+1
     DO 42 K=IIP1,N
       S=S+A(I1,K)*X(K,J)
     X(I1,J)={X(I1,J)-S}/A(I1,I1)
     KER=1
     RETURN
50  KER=2
   RETURN
END
SUBROUTINE MREAD(A,N,M,ND,MD,IREAD)
DIMENSION A(ND,MD),IREAD(10)
DO 10 I=1,N
10  READ(5,20)(A(I,J),J=1,M)

```



```

20 FORMAT(8F10.5)
RETURN
END
SUBROUTINE MWRITE(A,N,M,ND,MD,IWRITE)
DIMENSION A(ND,MD),IWRITE(10)
DO 10 I=1,N
DO 10 J=1,M
10 WRITE(6,20)(I,J,A(I,J),J=1,M)
20 FORMAT(6(3X,'(',I2,',',I2,',')= ',1PE10.3))
RETURN
END
//GO.F106F001 DD SPACE=(CYL,(6,1))
//GO.SYSIN DD *
4 2 12 12 12 10 1.
0.

```

```

28. 41.52 76. 41.52 41.52
41.52 76. 41.52 28.
1. 1. 1. 1. 1.
1. 1. 1. 1. 1.
1. 1. 1. 1. 1.

```


FILTER FOR TRACKING MANEUVERING AIRCRAFT

```

// EXEC FORTCLGP, REGION.GO=200K
// FORT
C THIS PROGRAM PERFORMS MONTE CARLO SIMULATION OF STATE ESTIMATORS
C OF WHICH THE KALMAN FILTER IS ONE EXAMPLE. THERE ARE SEVERAL
C OPTIONS AVAILABLE AS INDICATED IN THE DETAILLED COMMENTS BELOW.
C IT SHOULD BE NOTED THAT ALL COMPUTATIONS OF GAINS USING THE
C SUBROUTINE GAIN ARE PERFORMED IN DOUBLE PRECISION. THUS ALL
C ARRAYS FOR USE IN "GAIN" MUST BE PREPARED ACCORDINGLY.
C
C REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI
C COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C 1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C 2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,60), ERR(4,60),
C 3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C 4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), SIGV(4),
C 5XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C 6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITR0, IXZ, IV, IW, IEST, ND
C DIMENSION XP(80), YP(80)
C
C N=ORDER OF SYSTEM MODEL AND FILTER (DIMENSION OF X,XHAT)
C M=NUMBER OF MEASUREMENTS (DIMENSION OF THE VECTOR Z)
C IN=NUMBER OF INPUT RANDOM FORCING FCNS (=DIMENSION OF W)
C NSAM=NUMBER OF TIME SAMPLES
C NENS=NUMBER OF MEMBERS IN ENSEMBLE
C READ (5,81) N,M,IN,NSAM,NENS
C
C READ (5,32) ND
C THE VALUE OF ND READ IN MUST EQUAL THE ROW (AND COLUMN) DIMENSION
C SPECIFIED FOR THE SQUARE MATRIX "TEMPI", E.G. IF TEMPI(3,3) IS
C SPECIFIED IN THE COMMON STATEMENT "ND" MUST BE EQUAL TO 3.
C
C IG=-1 -- GAINS COMPUTED OFF-LINE AND READ IN
C 0 -- GAINS COMPUTED ONLY ONCE BEFORE STARTING MONTE CARLO
C 1 -- GAINS COMPUTED FOR EACH MEMBER OF ENSEMBLE
C
C IFLR=0 -- R IS READ IN
C IFLR.NE.0 -- R IS COMPUTED ON-LINE AT EACH TIME SAMPLE
C
C IEST=0 -- STANDARD KALMAN FILTER EQUATION IS USED
C IEST.NE.0 -- STD. KALMAN FILTER EQ. NOT USED

```

MCSPO0000
 MCSPO0001
 MCSPO0002
 MCSPO0003
 MCSPO0004
 MCSPO0005
 MCSPO0006
 MCSPO0007
 MCSPO0008
 MCSPO0009
 MCSPO0010
 MCSPO0011
 MCSPO0012
 MCSPO0014
 MCSPO0015
 MCSPO0016
 MCSPO0017
 MCSPO0018
 MCSPO0019
 MCSPO0020
 MCSPO0021
 MCSPO0022
 MCSPO0023
 MCSPO0024
 MCSPO0025
 MCSPO0026
 MCSPO0027
 MCSPO0028
 MCSPO0029
 MCSPO0030
 MCSPO0031
 MCSPO0032
 MCSPO0033
 MCSPO0034
 MCSPO0035
 MCSPO0036
 MCSPO0037
 MCSPO0038
 MCSPO0039
 MCSPO0040
 MCSPO0041
 MCSPO0042
 MCSPO0043
 MCSPO0044
 MCSPO0045


```

ISIGV=0 -- STD. DEVIATIONS OF MEASUREMENT NOISE TO BE READ IN (SP) MCSP00095
ISIGW=0 -- STD. DEVIATIONS OF RANDOM INPUTS TO BE READ IN (SP) MCSP00096
IXHZ=0 -- INITIAL VALUE OF THE PREDICTED VALUE XH(0/-1) TO MCSP00097
          BE READ IN (S.P.) MCSP00098
          MCSP00099
          MCSP0100
          MCSP0101
          MCSP0107
          MCSP0108
          MCSP0109
          MCSP0110
          MCSP0111
          MCSP0112
          MCSP0113
          MCSP0114
          MCSP0115
          MCSP0116
          MCSP0117
          MCSP0118
          MCSP0119
          MCSP0120
          MCSP0121
          MCSP0122
          MCSP0123
          MCSP0124
          MCSP0125
          MCSP0126
          MCSP0128
          MCSP0129
          MCSP0130
          MCSP0131
          MCSP0132
          MCSP0133
          MCSP0134
          MCSP0135
          MCSP0136
          MCSP0137
          MCSP0138
          MCSP0139
          MCSP0140
          MCSP0141
          MCSP0142
          MCSP0143
          MCSP0144
          MCSP0145
          MCSP0146
          MCSP0147

READ (5,86) IPHI,IH,IR,IPKKM1,IGAM,ISIGV,ISIGW,IXHZ,IC
CALL OVFLOW
IW = 6395217
IV = 1936743
IXZ = 135769

THE FOLLOWING SECTION PRINTS OUT A DESCRIPTION OF THE RUN AS
SPECIFIED BY THE USER'S FLAGS

WRITE (6,156)
WRITE (IG,EQ.0) GO TO 1
IF (IG,EQ.1) GO TO 2
WRITE (6,88)
GO TO 3
WRITE (6,89)
GO TO 3
WRITE (6,90)
IF (IEST,EQ.0) GO TO 4
WRITE (6,91)
GO TO 5
WRITE (6,92)
IF (ITRK,EQ.0) GO TO 8
IF (ITRK,EQ.-1) GO TO 7
IF (ITRO,EQ.0) GO TO 6
WRITE (6,93)
GO TO 9
WRITE (6,94)
GO TO 9
WRITE (6,95)
GO TO 9
WRITE (6,96)
IF (ISTAT,EQ.0) GO TO 10
WRITE (6,97)
GO TO 11
WRITE (6,98)
GO TO 13
IF (IQ,EQ.0) GO TO 12
IF (IQ,EQ.1) GO TO 12
WRITE (6,99)

```

```

CCCCCCCC
CCCCCCCC

```



```

12 GO TO 14 (6,100)
13 GO TO 14 (6,101)
14 IF (IFLR.EQ.0) GO TO 15
15 WRITE (6,102)
16 GO TO 16 (6,103)
17 WRITE (6,104)
18 IF (IPHI.EQ.0) WRITE (6,105)
19 IF (IPH.EQ.0) WRITE (6,106)
20 IF (IFLR.EQ.0) WRITE (6,107)
21 IF (IQ.EQ.0) GO TO 17
22 IF (IQ.EQ.-1) GO TO 18
23 WRITE (6,108)
24 GO TO 18 (6,109)
25 WRITE (6,110)
26 IF (ISIGV.EQ.0) WRITE (6,111)
27 IF (ISIGW.EQ.0) WRITE (6,112)
28 IF (ISIGZ.EQ.0) WRITE (6,113)
29 IF (IC.NE.1) WRITE (6,114)
30 IF (IPKMI.EQ.0) WRITE (6,115)

```

THE FOLLOWING SECTION PRINTS OUT A DESCRIPTION OF THE OUTPUT
DATA CALLED FOR

```

19 WRITE (6,116)
20 IF (IPRT.NE.0) GO TO 19
21 WRITE (6,117)
22 IF (IG.EQ.0) WRITE (6,118)
23 WRITE (6,119)
24 IF (ISIAF.NE.0) WRITE (6,120)
25 GO TO 20 (6,121)
26 WRITE (6,122)
27 IF (IPT.NE.0) GO TO 21
28 WRITE (6,123)
29 IF (IGPLP.EQ.1) WRITE (6,124)
30 IF (ITHVPL.EQ.1) WRITE (6,125)
31 IF (ITPPLT.EQ.1) WRITE (6,126)
32 IF (ISMPPLT.EQ.1) WRITE (6,127)
33 GO TO 22 (6,128)
34 WRITE (6,129)
35 CONTINUE
36 WRITE (6,130)

```

CCCCC

MCSP0148
MCSP0149
MCSP0150
MCSP0151
MCSP0152
MCSP0153
MCSP0154
MCSP0155
MCSP0156
MCSP0157
MCSP0158
MCSP0159
MCSP0160
MCSP0161
MCSP0162
MCSP0163
MCSP0164
MCSP0165
MCSP0166
MCSP0167
MCSP0168
MCSP0169
MCSP0170
MCSP0171
MCSP0172
MCSP0173
MCSP0174
MCSP0175
MCSP0176
MCSP0177
MCSP0178
MCSP0179
MCSP0180
MCSP0181
MCSP0182
MCSP0183
MCSP0184
MCSP0185
MCSP0186
MCSP0187
MCSP0188
MCSP0189
MCSP0190
MCSP0191
MCSP0192
MCSP0193
MCSP0194
MCSP0195


```

WRITE (6,129) N,M,IN,NSAM,NENS,ND
WRITE (6,130) N,M,IN,NSAM,NENS,ND

```

```

THE FOLLOWING SECTION READS THE SPECIFIED INPUT MATRICES

```

```

IF (IPHI.NE.0) GO TO 24
CALL MREAD (PHI,N,N)

```

```

DO 23 I=1,N

```

```

DO 23 J=1,N
23 PHIS(I,J) = PHI(I,J)

```

```

WRITE (6,131)
CALL MWRITE (PHI,N,N)

```

```

24 IF (IH.NE.0) GO TO 26
CALL MREAD (H,M,N)

```

```

DO 25 I=1,M

```

```

DO 25 J=1,N
25 HS(I,J) = H(I,J)

```

```

WRITE (6,132)
CALL MWRITE (H,M,N)

```

```

26 IF (IR.NE.0) GO TO 27
CALL MREAD (R,M,M)
WRITE (6,133)
CALL MWRITE (R,M,M)

```

```

27 IF (IQ.NE.1) GO TO 28
CALL MREAD (COVW,IN,IN)
WRITE (6,134)
CALL MWRITE (COVW,IN,IN)
GO TO 29

```

```

28 IF (IQ.NE.0) GO TO 29
CALL MREAD (Q,N,N)
WRITE (6,135)
CALL MWRITE (Q,N,N)

```

```

29 IF (IGAM.NE.0) GO TO 31

```

MCSP0196
 MCSP0197
 MCSP0198
 MCSP0199
 MCSP0200
 MCSP0201
 MCSP0202
 MCSP0203
 MCSP0204
 MCSP0205
 MCSP0206
 MCSP0207
 MCSP0208
 MCSP0209
 MCSP0210
 MCSP0211
 MCSP0212
 MCSP0213
 MCSP0214
 MCSP0215
 MCSP0216
 MCSP0217
 MCSP0218
 MCSP0219
 MCSP0220
 MCSP0221
 MCSP0222
 MCSP0223
 MCSP0224
 MCSP0225
 MCSP0226
 MCSP0227
 MCSP0228
 MCSP0229
 MCSP0230
 MCSP0231
 MCSP0232
 MCSP0233
 MCSP0234
 MCSP0235
 MCSP0236
 MCSP0237
 MCSP0238
 MCSP0239
 MCSP0240
 MCSP0241
 MCSP0242
 MCSP0243


```

C      CALL MREAD (GAMMA,N,IN)
C      DO 30 I=1,N
C
C      DO 30 J=1,IN
C      30 GAMMAS(I,J) = GAMMA(I,J)
C      WRITE (6,136)
C      CALL MWRITE (GAMMA,N,IN)
C
C      31 IF (IPKKM1.NE.0) GO TO 32
C      CALL MREAD (PKKM1,N,N)
C      WRITE (6,137)
C      CALL MWRITE (PKKM1,N,N)
C
C      32 IF (ISIGV.NE.0) GO TO 33
C      CALL VREAD (SIGV,M)
C      WRITE (6,138)
C      CALL VWRITE (SIGV,M)
C
C      33 IF (ISIGW.NE.0) GO TO 34
C      CALL VREAD (SIGW,IN)
C      WRITE (6,139)
C      CALL VWRITE (SIGW,IN)
C
C      34 IF (IXHZ.NE.0) GO TO 35
C      CALL VREAD (XHATZ,N)
C      WRITE (6,140)
C      CALL VWRITE (XHATZ,N)
C
C      35 IF (IC.EQ.1) GO TO 36
C      IC.NE.1 MEANS THAT MEANS AND STD. DEVIATIONS OF THE INITIAL STATE
C      VALUE MUST BE READ IN. OTHERWISE NOT READ IN.
C      CALL VREAD (XZMEAN,N)
C      WRITE (6,141)
C      CALL VWRITE (XZMEAN,N)
C
C      CALL VREAD (SIGXZ,N)
C      WRITE (6,142)
C      CALL VWRITE (SIGXZ,N)
C      GO TO 40
C

```

```

MCSP0244
MCSP0245
MCSP0246
MCSP0247
MCSP0248
MCSP0249
MCSP0250
MCSP0251
MCSP0252
MCSP0253
MCSP0254
MCSP0255
MCSP0256
MCSP0257
MCSP0258
MCSP0259
MCSP0260
MCSP0261
MCSP0262
MCSP0263
MCSP0264
MCSP0265
MCSP0266
MCSP0267
MCSP0268
MCSP0269
MCSP0270
MCSP0271
MCSP0272
MCSP0273
MCSP0274
MCSP0275
MCSP0276
MCSP0277
MCSP0278
MCSP0279
MCSP0280
MCSP0281
MCSP0282
MCSP0283
MCSP0284
MCSP0285
MCSP0286
MCSP0287
MCSP0288
MCSP0289
MCSP0290
MCSP0291

```



```

C      36 READ (5,144) (XS(I,1),I=1,N)
C      INITIAL CONDITION HAS BEEN READ
C      WRITE (6,143) (XS(I,1),I=1,N)
C      IF (ITRK.NE.1) GO TO 40
C      IF (ITRU.NE.0) GO TO 38
C
C      37 DO 37 K=2,NSAM
C      READ (5,144) (XS(I,K),I=1,N)
C
C      GO TO 39
C      38 CALL TRACK
C      IF TRACK CALLED HERE IT SHOULD BE WRITTEN TO GENERATE AND
C      STORE THE TRACK IN XS(N,K) FOR K=2(NSAM),NSAM
C
C      39 WRITE (6,145) (XS(I,1),I=1,N)
C      WRITE (6,146) (XS(I,NSAM),I=1,N)
C      40 CONTINUE
C
C      THE FOLLOWING SECTION PREPARES FOR THE MONTE CARLO LOOP
C      FORM NXN IDENTITY MATRIX IN DOUBLE PRECISION
C
C      DO 41 I=1,N
C
C      DO 41 J=1,N
C      EI(I,J)=0.DO
C      IF (I.EQ.J) EI(I,J)=1.DO
C
C      41 GIVEN THE MATRIX GAMMA AND THE COVARIANCE OF W COMPUTE Q
C      USING DOUBLE PRECISION ARITHMETIC
C      IF (IQ.NE.1) GO TO 42
C      CALL QMAT
C      WRITE (6,135)
C      CALL MWRITE(Q,N,N)
C      42 IF (IG.NE.-1) GO TO 44
C
C      DO 43 K=1,NSAM
C
C      DO 43 I=1,N
C      43 READ (5,144) (GKS(I,J,K),J=1,M)
C
C      GO TO 47
C      44 IF (IG.NE.0) GO TO 47
C

```



```

C      DO 46 K=1,NSAM
C      CALL GAIN
C
C      DO 46 I=1,N
C
C      DO 45 L=1,N
C      PKKS(I,L,K) = PKK(I,L)
C
C      DO 46 J=1,M
C      GKS(I,J,K) = G(I,J)
C
C      47 CONTINUE
C      IF GAINS WERE TO BE READ IN (IG=-1) OR COMPUTED ONLY
C      ONCE(IG=0), THIS HAS NOW BEEN DONE
C
C      SET UP ARRAYS FOR COMPUTING STATISTICS
C
C      DC 48 K=1,NSAM
C
C      DO 48 J=1,N
C      XM(J,K) = 0.
C      ERR(J,K) = 0.
C
C      DO 48 L=1,N
C      48 VAR(J,L,K) = 0.
C
C      BEGIN MAIN ITERATION LOOP HERE
C
C      DC 54 ITER=1,NENS
C      IF (IC.EQ.1) GO TO 49
C      CALL XZERO
C
C      49 DO 50 I=1,N
C      50 XHKKM1(I) = XHATZ(I)
C
C      DO 54 K=1,NSAM
C      FORM NOISY MEASUREMENT FROM TRUE STATE VALUE
C
C      DO 51 I=1,N
C      51 X(I) = XS(I,K)
C      CALL MEAS

```

```

MCSP0340
MCSP0341
MCSP0342
MCSP0343
MCSP0344
MCSP0345
MCSP0346
MCSP0347
MCSP0348
MCSP0349
MCSP0350
MCSP0351
MCSP0352
MCSP0353
MCSP0354
MCSP0355
MCSP0356
MCSP0357
MCSP0358
MCSP0359
MCSP0360
MCSP0361
MCSP0362
MCSP0363
MCSP0364
MCSP0365
MCSP0366
MCSP0367
MCSP0368
MCSP0369
MCSP0370
MCSP0371
MCSP0372
MCSP0373
MCSP0374
MCSP0375
MCSP0376
MCSP0377
MCSP0378
MCSP0379
MCSP0380
MCSP0381
MCSP0382
MCSP0383
MCSP0384
MCSP0385
MCSP0386
MCSP0387

```



```

C      GAIN IS NOT TO BE COMPUTED ON-LINE IF IG.NE.1
C      IF (IG.NE.1) GO TO 53
C
C      Q IS TO BE COMPUTED ON-LINE IF IFLQ.NE.0
C      IF (IFLQ.NE.0) CALL QON
C      R IS TO BE COMPUTED ON-LINE IF IFLR.NE.0
C
C      IF (IFLR.NE.0) CALL RON
C      CALL GAIN
C
C      DO 52 I=1,N
C
C      DO 52 J=1,M
C      52 GKS(I,J,K) = G(I,J)
C
C      UPDATE THE STATE ESTIMATE
C
C      53 CALL ESTIM
C
C      UPDATE RUNNING SUMS USED IN COMPUTING STATISTICS
C      CALL STAT
C      IF (K.EQ.NSAM) GO TO 54
C
C      UPDATE TRACK BY COMPUTING X(K+1)
C      IF (ITRK.NE.1) CALL TRACK
C      54 CONTINUE
C
C      DIVIDE RUNNING SUMS COMPUTED BY SUBROUTINE STAT BY ENSEMBLE
C      SIZE TO COMPUTE STATISTICS
C      ENS = NENS
C
C      DO 56 K=1,NSAM
C
C      DO 56 J=1,N
C      IF (ITRK.EQ.1) GO TO 55
C      XM(J,K) = XM(J,K)/ENS
C      55 ERR(J,K) = ERR(J,K)/ENS
C      56 VAR(J,J,K) = VAR(J,J,K)/ENS-ERR(J,K)**2
C
C      IF (ISTAT.EQ.0) GO TO 58
C
C      COMPUTE OFF-DIAGONAL TERMS IN COVARIANCE OF ESTIMATION
C      ERROR MATRIX IF ISTAT.NE.0
C      DO 57 K=1,NSAM

```

```

MC SP0388
MC SP0389
MC SP0390
MC SP0391
MC SP0392
MC SP0393
MC SP0394
MC SP0395
MC SP0396
MC SP0397
MC SP0398
MC SP0399
MC SP0400
MC SP0401
MC SP0402
MC SP0403
MC SP0404
MC SP0405
MC SP0406
MC SP0407
MC SP0408
MC SP0409
MC SP0410
MC SP0411
MC SP0412
MC SP0413
MC SP0414
MC SP0415
MC SP0416
MC SP0417
MC SP0418
MC SP0419
MC SP0420
MC SP0421
MC SP0422
MC SP0423
MC SP0424
MC SP0425
MC SP0426
MC SP0427
MC SP0428
MC SP0429
MC SP0430
MC SP0431
MC SP0432
MC SP0433
MC SP0434
MC SP0435

```



```

C      DO 57 L=2,N
      LM1 = L-1
      MCSP0436
      MCSP0437
      MCSP0438
      MCSP0439
      MCSP0440
      MCSP0441
      MCSP0442
      MCSP0443
      MCSP0444
      MCSP0445
      DO 57 J=1,LM1
      57 VAR(L,J,K) = VAR(L,J,K)/ENS-ERR(L,K)*ERR(J,K)
      MCSP0489
      MCSP0490
      58 CONTINUE
      IF (IPRT.NE.0) GO TO 64
      CALL PRT
      64 IF (IPLT.NE.0) GO TO 80
      CALL PLT
      80 CONTINUE
      STOP
      C
      81 FORMAT (5(I10))
      82 FORMAT (I2)
      83 FORMAT (7(I10))
      84 FORMAT (2(I15))
      85 FORMAT (5(I10))
      86 FORMAT (9I5)
      87 FORMAT (20X,'DESCRIPTION OF RUN',//)
      88 FORMAT (10X,'GAINS COMPUTED OFF-LINE AND READ IN',//)
      89 FORMAT (10X,'GAINS COMPUTED ONCE IN "GAIN" BEFORE STARTING MONTE CARLO',//)
      90 FORMAT (10X,'GAINS COMPUTED FOR EACH MEMBER OF ENSEMBLE',//)
      91 FORMAT (10X,'THE STANDARD LINEAR EQS. DO NOT CHARACTERIZE THE FILTER',//)
      92 FORMAT (10X,'THE STD. KALMAN EQS. CHARACTERIZE THE LINEAR FILTER',//)
      93 FORMAT (10X,'ONLY ONE TRACK IS USED AND IT IS GENERATED BY SUBROUTINE TRACK',//)
      94 FORMAT (10X,'ONLY ONE TRACK IS USED AND IT IS READ IN',//)
      95 FORMAT (10X,'SEVERAL TRACKS USED BUT NOT GENERATED FROM STD. LINEAR DIFFERENCE EQS.',//)
      96 FORMAT (10X,'SEVERAL TRACKS GENERATED BY USING THE STD. LINEAR DIFFERENCE EQS.',//)
      97 FORMAT (10X,'MEAN OF TRACK, MEAN OF EST. ERROR AND COVARIANCE OF EST. ERROR ARE COMPUTED',//)
      98 FORMAT (10X,'MEAN OF TRACK, MEAN AND VARIANCES OF EST. ERROR ARE COMPUTED',//)
      99 FORMAT (10X,'THE Q MATRIX IS COMPUTED ON-LINE AT EACH SAMPLE BY "QMCON"',//)
      100 FORMAT (10X,'THE COVARIANCE OF W IS READ IN AND Q IS COMPUTED BY "IQMAT" BEFORE STARTING MONTE CARLO',//)
      101 FORMAT (10X,'THE Q MATRIX IS READ IN',//)
      MCSP0552
      MCSP0553
      MCSP0554
      MCSP0555
      MCSP0556
      MCSP0557
      MCSP0558
      MCSP0560
      MCSP0561
      MCSP0562
      MCSP0563
      MCSP0564
      MCSP0565
      MCSP0566
      MCSP0567
      MCSP0568
      MCSP0569
      MCSP0570
      MCSP0571
      MCSP0572
      MCSP0573
      MCSP0574
      MCSP0575
      MCSP0576
      MCSP0577
      MCSP0578
      MCSP0579
      MCSP0580
      MCSP0581
      MCSP0582
      MCSP0583
      MCSP0584
      MCSP0585

```



```

146 FORMAT (9(2X,1PE12.5),/)
156 FORMAT ('1')
END
SUBROUTINE QMAT

```

CCCCCCCC

THIS SUBROUTINE COMPUTES THE MATRIX Q FROM THE EQUATION

Q=GAMMA* E(W*WT) * GAMMAT

DOUBLE PRECISION ARITHMETIC IS USED

```

REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VIMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,IIRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND

```

CC

```

CALL PROCD (GAMMA,COVW,N,IN,IN,TEMP)
CALL TRANS (GAMMA,N,IN,TEMP1)
CALL PROCD (TEMP,TEMP1,N,IN,N,Q)
RETURN
END
SUBROUTINE QON

```

CCCC

IF Q IS TO BE COMPUTED ON-LINE (IFLQ.NE.0) IT IS DONE
IN THIS SUBROUTINE

```

REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VIMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,IIRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND

```

CCCC

THE APPROPRIATE STATEMENTS FOR COMPUTING Q ON-LINE MUST
BE INSERTED HERE BY THE USER

```

RETURN
END
SUBROUTINE RON

```

C

MCSP0654
MCSP0764
MCSP0765
MCSP0766
MCSP0767
MCSP0768
MCSP0769
MCSP0770
MCSP0771
MCSP0772
MCSP0773
MCSP0774
MCSP0775
MCSP0776
MCSP0777
MCSP0778

MCSP0780
MCSP0781
MCSP0782
MCSP0783
MCSP0784
MCSP0785
MCSP0786
MCSP0787
MCSP0788
MCSP0789
MCSP0790
MCSP0791
MCSP0792
MCSP0793
MCSP0794
MCSP0795
MCSP0796
MCSP0797
MCSP0798

MCSP0800
MCSP0801
MCSP0802
MCSP0803
MCSP0804
MCSP0805
MCSP0806
MCSP0807
MCSP0808


```

C C C
IF R IS TO BE COMPUTED ON-LINE (IFLR.NE.O) IT IS DONE
IN THIS SUBROUTINE
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
ITEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),VIMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,I,ITER,K,ITRO,IXZ,IV,IW,IEST,ND

THE APPROPRIATE STATEMENTS FOR COMPUTING R CN-LINE MUST
BE INSERTED HERE BY THE USER

RETURN
END
SUBROUTINE STAT
THIS SUBROUTINE STAT COMPUTES RUNNING SUMS USED IN DETERMINING THE
SAMPLE STATISTICS OF TRACK AND ESTIMATION ERRORS. IN THE DEFAULT
OPTION (IESTAT.EQ.O) THE STATISTICS TO BE COMPUTED ARE MEAN OF
TRACK, MEAN OF ESTIMATION ERROR AND VARIANCE OF ESTIMATION
ERROR. IF (IESTAT.NE.O) THE OFF-DIAGONAL TERMS IN THE COVARIANCE OF
ESTIMATION ERROR MATRIX ARE ALSO COMPUTED.
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,PKKM1,G,PKK,Q,EI
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
ITEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),VIMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,I,ITER,K,ITRO,IXZ,IV,IW,IEST,ND
DIMENSION IQ,EXH(3)
IF (ITER.NE.1) GO TO 2
IF (ITER.NE.1) GO TO 4
DO 1 J=1,N
1 XM(J,K) = XS(J,K)
GO TO 4
2 CONTINUE
DO 3 J=1,N
3 XM(J,K) = XM(J,K)+XS(J,K)
4 CONTINUE
DC 5 J=1,N

```

MCSP0809
MCSP0810
MCSP0811
MCSP0812
MCSP0813
MCSP0814
MCSP0815
MCSP0816
MCSP0817

MCSP0819
MCSP0820
MCSP0821
MCSP0822
MCSP0823
MCSP0824
MCSP0825
MCSP0826
MCSP0827
MCSP0828
MCSP0829
MCSP0830
MCSP0831
MCSP0832
MCSP0833
MCSP0834
MCSP0835
MCSP0836
MCSP0837
MCSP0838

MCSP0840
MCSP0841
MCSP0842
MCSP0843
MCSP0844
MCSP0845
MCSP0846
MCSP0847
MCSP0848
MCSP0849
MCSP0850
MCSP0851
MCSP0852
MCSP0853
MCSP0854
MCSP0855
MCSP0856


```

C      EXH(J) = XHKK(J)-XS(J,K)
C      ERR(J,K) = ERR(J,K)+EXH(J)
5      VAR(J,J,K) = VAR(J,J,K)+EXH(J)**2
C
C      IF (ISTAT.EQ.0) RETURN
C
C      DO 6 L=2,N
C      LM1 = L-1
C
C      DO 6 J=1,LM1
C      6      VAR(L,J,K) = VAR(L,J,K)+EXH(L)*EXH(J)
C      RETURN
C
C      SUBROUTINE XZERO
C      THIS SUBROUTINE GENERATES THE INITIAL STATE VALUE FROM A NORMAL
C      RANDOM NUMBER GENERATOR. IT IS ASSUMED THAT THE INITIAL STATE
C      RANDOM NUMBERS THAT ARE INDEPENDENT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      2VAR(4,4,60),GKS(4,4,60),XS(4,60),HS(4,4),GK(4,4),SIGH(4,4),X(4),
C      3GAMMAS(4,4),PHIS(4,4),XSKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
C      4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),
C      5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
C      6N,NSAM,IQ,M,IIRK,IN,ISTAT,K,IIRQ,IXZ,IV,IN,IEST,ND
C      CALL SNORM (IXZ,X,N)
C
C      DO 1 I=1,N
C      1      XS(I,I) = SIGXZ(I)*X(I)+XZMEAN(I)
C      RETURN
C      END
C      SUBROUTINE ADD (A,B,N,M,C)
C      THIS SUBROUTINE ADDS THE NXM MATRICES A AND B, STORING THE
C      RESULT IN C
C      REAL*8 A,B,C
C      DIMENSION A(4,4),B(4,4),C(4,4)
C
C      DO 1 I=1,N
C
C      DO 1 J=1,M
C      1      C(I,J) = A(I,J)+B(I,J)
C      RETURN
C      END
C      SUBROUTINE MREAD (A,N,M)
C      80DIC.5. THE ENTRIES IN THE FIRST ROW OF A ARE READ FIRST, THEN

```



```

C      THIS SUBROUTINE READS AN NXM MATRIX A ACCORDING TO THE FORMAT
C      THE ENTRIES IN THE SECOND ROW, AND SO ON.
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DO 1 I=1,N
C      1 READ (5,2) (A(I,J),J=1,M)
C      RETURN
C
C      2 FORMAT (8F10.0)
C      END
C      SUBROUTINE MWRITE (A,N,M)
C      THIS SUBROUTINE WRITES THE ENTRIES OF THE NXM MATRIX A
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DO 1 I=1,N
C      1 WRITE (6,2) (A(I,J),J=1,M)
C      RETURN
C
C      2 FORMAT (9(2X,1PE12.5))
C      END
C      SUBROUTINE PROD (A,B,N,M,L,C)
C      THIS SUBROUTINE COMPUTES THE MATRIX PRODUCT AB AND STORES THE
C      RESULT IN C
C      A = NXM, B = NXL, C = NXL
C      REAL*8 A,B,C,T
C      DIMENSION A(4,4),B(4,4),C(4,4),T(4,4)
C
C      DO 1 I=1,N
C      DO 1 J=1,L
C      1 T(I,J) = 0.0
C
C      DO 2 I=1,N
C      DO 2 J=1,L
C      DO 2 K=1,M
C      2 T(I,J) = T(I,J)+A(I,K)*B(K,J)
C
C      DO 3 I=1,N
C      DO 3 J=1,L

```

MCSP0967
 MCSP0969
 MCSP0970
 MCSP0971
 MCSP0972
 MCSP0973
 MCSP0974
 MCSP0975
 MCSP0976
 MCSP0977
 MCSP0978
 MCSP0979
 MCSP0980
 MCSP0981
 MCSP0982
 MCSP0983
 MCSP0984
 MCSP0985
 MCSP0986
 MCSP0987
 MCSP0988
 MCSP0989
 MCSP0990
 MCSP0991
 MCSP0992
 MCSP0993
 MCSP0994
 MCSP0995
 MCSP0996
 MCSP0997
 MCSP0998
 MCSP0999
 MCSP1000
 MCSP1001
 MCSP1002
 MCSP1003
 MCSP1004
 MCSP1005
 MCSP1006
 MCSP1007
 MCSP1008
 MCSP1009
 MCSP1010
 MCSP1011
 MCSP1012
 MCSP1013
 MCSP1014
 MCSP1015


```

3 C(I,J) = T(I,J)
RETURN
END
SUBROUTINE SUB (A,B,N,M,C)
THIS SUBROUTINE SUBTRACTS THE NXM MATRIX B FROM THE NXM MATRIX
A AND STORES THE RESULT IN C
REAL*8 A,B,C
DIMENSION A(4,4),B(4,4),C(4,4)
DO 1 I=1,N
DO 1 J=1,M
1 C(I,J) = A(I,J)-B(I,J)
RETURN
END
SUBROUTINE TRANS (A,N,M,C)
THIS SUBROUTINE FORMS THE MATRIX TRANSPOSE OF A STORING THE
RESULT IN C
REAL*8 A,C
DIMENSION A(4,4),C(4,4)
DO 1 I=1,N
DO 1 J=1,M
1 C(J,I) = A(I,J)
RETURN
END
SUBROUTINE VADD (X,Y,N,Z)
THIS SUBROUTINE COMPUTES THE SUM OF THE N-VECTORS X AND
Y AND STORES THE RESULT IN THE N-VECTOR Z
REAL*4 X(4),Y(4),Z(4)
DO 1 I=1,N
1 Z(I) = X(I)+Y(I)
RETURN
END
SUBROUTINE VPROD (A,X,M,N,Y)
THIS SUBROUTINE COMPUTES THE PRODUCT OF THE MXN MATRIX
A AND THE N-VECTOR X AND STORES THE RESULT IN THE
M-VECTOR Y

```



MCSP1064
MCSP1065
MCSP1066
MCSP1067
MCSP1068
MCSP1069
MCSP1070
MCSP1071
MCSP1072
MCSP1073
MCSP1074
MCSP1075
MCSP1076
MCSP1077
MCSP1078
MCSP1079
MCSP1080
MCSP1081
MCSP1082
MCSP1083

```

C      REAL*4 A(4,4),X(4),Y(4),T(4)
C      DC 1 I=1,M
C      T(I) = 0.DO
C
C      DC 1 J=1,N
C      1 T(I) = T(I)+A(I,J)*X(J)
C
C      DC 2 I=1,M
C      2 Y(I) = T(I)
C      RETURN
C      ENC
C      SUBROUTINE VREAD (V,N)
C
C      THIS SUBROUTINE READS THE N-DIMENSIONAL S.P. VECTOR V
C
C      DIMENSION V(4)
C      READ (5,1) (V(I),I=1,N)
C      RETURN
C      1 FORMAT (8F10.0)
C      END
C      SUBROUTINE VSUB (X;Y,N,Z)
C      REAL*4 X(4),Y(4),Z(4)
C      DC 1 I=1,N
C      1 Z(I) = X(I)-Y(I)
C      RETURN
C      END
C      SUBROUTINE VWRITE (V,N)
C      DIMENSION V(4)
C      WRITE (6,1) (V(I),I=1,N)
C      RETURN
C      1 FORMAT (9(2X,1PE12.5))
C      END

```

MCSP0871
MCSP0872
MCSP0873
MCSP0874
MCSP0875
MCSP0876
MCSP0877
MCSP0878
MCSP0879
MCSP0880
MCSP0881
MCSP0882
MCSP0883

```

C      SUBROUTINE TRACK
C      IF TRACK IS TO BE GENERATED ON-LINE IT IS DCNE IN THIS SUBROUTINE
C      IN THE DEFAULT OPTION (ITRK.EQ.0) THE TRACK IS GENERATED
C      FROM THE STANDARD LINEAR DIFFERENCE EQUATION
C
C      X(K+1)=PHI*X(K)+GAMMA*W(K)
C
C      REAL*8 GAMMA,COVM,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),GAMMA(4,4),COVM(4,4),
C      1 TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      2 VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      3 GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
C      4 SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),V(4),SIGV(4),

```



```

5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND
DIMENSION N(3)
ITRK NE.0 OR 1 -- SEVERAL TRACKS GENERATED,BUT NOT FROM STD.
= 0 -- SEVERAL TRACKS GENERATED FROM STD LINEAR EQS
= 1 -- ONLY ONE TRACK IS USED
IF (ITRK.NE.0) GO TO 4
CALL SNORM(IW,W,IN)
CCONVERT EACH N(0,1) R.V. TO N(0,SIGW(I)) R.V.

DO 1 I=1,IN
1 W(I) = SIGW(I)*W(I)

DO 2 I=1,N
2 X(I) = XS(I,K)

CALL VPROD (GAMMAS,W,N,IN,W)
CALL VPROD (PHIS,X,N,N,VTMP)
CALL VADD (VTMP,W,N,VTMP)

DO 3 I=1,N
3 XS(I,K+1) = VTMP(I)

NEW VALUE OF X HAS BEEN COMPUTED AND STORED IN THE ARRAY XS
RETURN
4 IF (ITRK.NE.1) GO TO 6
IF (ITRK.EQ.1) THE USER MUST INSERT HERE THE STATEMENTS REQUIRED
TO GENERATE A SINGLE TRAJECTORY AND STORE IT IN THE ARRAY
XS(I,K),I=1,N,K=2,NSAM (NOTE THAT IF A SINGLE TRAJECTORY IS TO BE
GENERATED, THE INITIAL CONDITION HAS BEEN READ IN AND STORED
IN XS(I,1),I=1,N)

TPI = 2.*3.14159265
DO 5 K=2,NSAM
EKM1 = K-1
T = 1.0*EKM1
A=0.03333*T
IF(A.LT.TPI) GO TO 10
FM=A/TPI
FM=MM
A = A - FM*TPI
10 CONTINUE
XS(1,K)=10.*SIN(A)
XS(2,K)=.3333*COS(A)
XS(3,K)=10.*COS(A)
5 XS(4,K)=-.3333*SIN(A)

```

MCSP0885
 MCSP0886
 MCSP0887
 MCSP0888
 MCSP0889
 MCSP0890
 MCSP0891
 MCSP0892
 MCSP0893
 MCSP0894
 MCSP0895
 MCSP0896
 MCSP0897
 MCSP0898
 MCSP0899
 MCSP0900
 MCSP0901
 MCSP0902
 MCSP0903
 MCSP0904
 MCSP0905
 MCSP0906
 MCSP0907
 MCSP0908
 MCSP0909
 MCSP0910
 MCSP0911
 MCSP0912
 MCSP0913
 MCSP0914
 MCSP0915
 MCSP0916
 MCSP0917

 MCSP0918
 MCSP0919




```

C      RETURN
C      IF CONTINUE POINT IS REACHED, ITRK NOT EQUAL 0 CR 1 INDICATING THAT
C      IF SEVERAL TRACKS ARE TO BE GENERATED, BUT NOT BY USING THE STD.
C      LINEAR DIFFERENCE EQS..THE USER MUST SUPPLY THE APPROPRIATE
C      STATEMENTS HERE.
C      RETURN
C      END
C      SUBROUTINE MEAS
C      THIS SUBROUTINE STARTS WITH THE TRUE STATE VALUE XS
C      AND ADDS ZERO-MEAN WHITE GAUSSIAN NOISE TO H*XS TO
C      GENERATE A NOISY VECTOR OF MEASUREMENTS Z.
C
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C      4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
C      5XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND
C      ALPHA = XS(3,K)
C      BETA = XS(1,K)
C      Z(1) = SQRT(ALPHA**2+BETA**2)
C      Z(2) = ATAN2(ALPHA,BETA)
C      CALL SNCRM (IV,V,M)
C
C      DO 1 I=1,M
C      1 V(I) = SIGV(I)*V(I)
C
C      CALL VADD (Z,V,M,Z)
C      ALPHA = Z(1)*COS(Z(2))
C      BETA = Z(1)*SIN(Z(2))
C      XZ(K)=ALPHA
C      YZ(K)=BETA
C      RETURN
C      END
C      SUBROUTINE GAIN
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4),
C      1TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), PHI(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,60),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,4), GK(4,4), SIGW(4), X(4),
C      4SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTMP(4), Z(4), V(4), SIGV(4),
C      5XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND

```

MCSP0925
 MCSP0926
 MCSP0927
 MCSP0928
 MCSP0929
 MCSP0930
 MCSP0931
 MCSP0932
 MCSP0933
 MCSP0734
 MCSP0735
 MCSP0736
 MCSP0737
 MCSP0738
 MCSP0739
 MCSP0740
 MCSP0741
 MCSP0742
 MCSP0743
 MCSP0744
 MCSP0745

MCSP0747
 MCSP0748
 MCSP0749
 MCSP0750
 MCSP0751
 MCSP0752
 MCSP0753
 MCSP0754
 MCSP0755
 MCSP0756
 MCSP0757
 MCSP0758
 MCSP0759

MCSP0762
 MCSP0763
 MCSP0695
 MCSP0696
 MCSP0697
 MCSP0698
 MCSP0699
 MCSP0700
 MCSP0701
 MCSP0703



```

C
C
C      DIMENSION BE(4),ER(4)
C      G(K) = P(K/K-1)*HT*(H*P(K/K-1)*HT + R)
C      DO 300 I=1,4
C      DO 300 J=1,4
C      PKKS(I,J,K)=PKKM1(I,J)
C      PX(1)=0.
C      PY(1)=0.
C      PX(2)=10.
C      PY(2)=10.
C      IF(DABS(PKKM1(1,1)-PKKM1(3,3)).GT.0) GO TO 11
C      PKKM1(1,1)=PKKM1(3,3)+0.000001
C      11 CONTINUE
C      THE=0.5*DATAN(2.*PKKM1(1,3)/(PKKM1(1,1)-PKKM1(3,3)))
C      IF(ABS(THE).GT.0) GO TO 10
C      THE = 0.00001
C      10 CCNTINUE
C      SIG2X=(PKKM1(1,1)+PKKM1(3,3))/2.+PKKM1(1,3)/SIN(2.*THE)
C      SIG2Y=(PKKM1(1,1)+PKKM1(3,3))/2.-PKKM1(1,3)/SIN(2.*THE)
C      DO 9 IN=1,2
C      IF(ABS(XHKKM1(1)-PX(IN)).GT.0) GO TO 9
C      XHKKM1(1)=0.000001+PX(IN)
C      9 BE(IN)=ATAN(XHKKM1(3)-PY(IN))/(XHKKM1(1)-PX(IN))
C      IF(SIG2X-GE.SIG2Y) GO TO 63
C      THE=THE+3.14159265/2.
C      CCNTINUE
C      63 DO 4 IN=1,2
C      66 ER(IN)=ABS(THE-BE(IN))
C      4 IF(ABS(COS(ER(1))).LE.ABS(COS(ER(2)))) GO TO 7
C      IN=1
C      GC TO 8
C      7 IN=2
C      8 XIN=IN
C      RR = ((XHKKM1(1)-PX(IN))**2+(XHKKM1(3)-PY(IN))**2)**.5
C      146 WRITE (6,146) THE,SIG2X,SIG2Y,BE(1),BE(2),XIN,ER(1),ER(2), RR
C      FORMAT (9(2X,1PE12.5),/)
C      H(1,1)=(XHKKM1(1)-PX(IN))/RR
C      H(1,3)=(XHKKM1(3)-PY(IN))/RR
C      CALL TRANS (H,M,N,TEMP2)
C      CALL PROD (PKKM1,TEMP2,N,M,TEMP)
C      CALL PROD (H,TEMP,M,N,M,TEMP1)
C      CALL ADD (TEMP1,R,M,M,TEMP1)
C      IF (M.EQ.1) GO TO 2
C      MD = ND
C      CALL GAUSS3 (M,EPS,TEMP1,TEMP2,KER,MD)
C      CALL PROD (TEMP,TEMP2,N,M,M,G)
C      NOTE HERE PKK(I,J) = P(K/K) WHERE
C
C
C      MCSP0704
C      MCSP0705
C
C      MCSP0634
C
C      MCSP0706
C      MCSP0707
C      MCSP0708
C      MCSP0709
C      MCSP0710
C      MCSP0711
C      MCSP0712
C      MCSP0713
C      MCSP0714
C      MCSP0715

```



```

C      P(K/K) = (I-G(K)*H)*P(K/K-1)
C      CALL PRCD (G,H,N,M,N,TEMP)
C      CALL SUB (EI,TEMP,N,N,TEMP2)
C      CALL PROD (TEMP2,PKKM1,N,N,N,PKK)
C
C      NOTE HERE   PKKM1(I,J) = P(K/K-1)   WHERE
C      P(K/K-1) = PHI*P(K-1/K-1)*PHIT + Q
C      CALL TRANS (PHI,N,N,TEMP2)
C      CALL PRCD (PKK,TEMP2,N,N,N,TEMP)
C      CALL PROD (PHI,TEMP,N,N,N,TEMP1)
C      CALL ADD (TEMP1,Q,N,N,PKKM1)
C      RETURN
C
C      DO 3 I=1,N
C      3 G(I,1) = TEMP(I,1)/TEMP1(1,1)
C
C      GC TO 1
C      END
C      SUBROUTINE ESTIM
C      THIS SUBROUTINE UPDATES THE STATE ESTIMATE. IN THE DEFAULT
C      CONDITION (TEST.EQ.0) THE STANDARD EQUATIONS
C
C      XHAT(K/) = XHAT(K/K-1) + G(K) * (Z(K) - H(K) * XHAT(K/K-1))
C
C      XHAT(K+1/K) = PHI * XHAT(K/K)
C
C      ARE EVALUATED
C      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), R(4,4), PHI(4,4),
C      1 TEMP(4,4), TEMP1(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), X(4,4), X(4,4), X(4,4),
C      2 VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,60), ERR(4,60), X(4), X(4),
C      3 GAMMAS(4,4), PHIS(4,4), XS(4,60), HS(4,60), GKI(4,4), SIGW(4), V(4), SIGV(4),
C      4 SIGXZ(4), XZMEAN(4), XHKK(4), PX(10), PY(10),
C      5 XHATZ(4), XZ(60), YZ(60), PX(10), PY(10),
C      6 N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITR0, IXZ, IV, IW, IEST, ND
C      TAKE THE APPROPRIATE GAIN AND STORE IN THE ARRAY GK
C
C      XIN=IN
C      DO 1 I=1,N
C      DO 1 J=1,M
C      1 GK(I,J) = GKS(I,J,K)
C
C      IF (TEST.NE.0) GO TO 2
C      CALL VPROD (HS,XHKKM1,M,N,VTMP)
C      VTMP(1) = ((XHKKM1(1)-PX(IN))**2 + (XHKKM1(3)-PY(IN))**2)**.5
C      Z(1) = (((XZ(K)-PX(IN))**2 + (YZ(K)-PY(IN))**2)**.5
C      CALL VSUB (Z,VTMP,M,VTMP)

```




```

C      CALL VPROD (GK,VTMP,N,M,VTMP)
C      CALL VADD (XHKKM1,VTMP,N,XHKK)
C
C      XHAT(K/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKK
C      CALL VPROD (PHIS,XHKK,N,N,XHKKM1)
C
C      XHAT(K+1/K) HAS BEEN COMPUTED AND STORED IN THE ARRAY XHKKM1
C      RETURN
C
C      2 CONTINUE
C      IF STANDARD EQUATIONS ARE NOT TO BE USED, THE APPROPRIATE
C      EQUATIONS MUST BE INSERTED HERE BY THE USER.
C      RETURN
C      END
C      SUBROUTINE PRI
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
C      1TEMP(4,4),TEMP1(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,60),ERR(4,60),
C      3GAMMAS(4,4),PHIS(4,4),XS(4,60),HS(4,60),SIGW(4),X(4),
C      4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VTMP(4),Z(4),SIGV(4),
C      5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10),
C      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IFEST,ND
C      IG=0
C      ISTAT=1
C      WRITE (6,147)
C      WRITE GAINS, THEORETICAL COVARIANCES OF ESTIMATION ERROR
C      IF ONE SET OF GAINS HAS BEEN USED.
C      IF (IG.NE.0) GO TO 61
C      WRITE (6,148)
C
C      DO 59 K=1,NSAM
C      WRITE (6,149) K
C
C      DO 59 I=1,N
C      WRITE (6,146) (GKS(I,J,K),J=1,M)
C
C      WRITE (6,150)
C
C      DO 60 K=1,NSAM
C      WRITE (6,151) K
C
C      DO 60 I=1,N
C      WRITE (6,146) (PKKS(I,J,K),J=1,N)
C
C      61 WRITE (6,156)
C      WRITE (6,152)

```

MCSP0682
MCSP0683
MCSP0684
MCSP0685
MCSP0686
MCSP0687
MCSP0688
MCSP0689
MCSP0690
MCSP0691
MCSP0692
MCSP0693
MCSP0694

MCSP0878
MCSP0879
MCSP0880
MCSP0881
MCSP0882
MCSP0883
MCSP0885

MCSP0446
MCSP0447
MCSP0448
MCSP0449
MCSP0450
MCSP0451
MCSP0452
MCSP0453
MCSP0454
MCSP0455
MCSP0456
MCSP0457
MCSP0458
MCSP0459
MCSP0460
MCSP0461
MCSP0462
MCSP0463
MCSP0464
MCSP0465
MCSP0466
MCSP0467
MCSP0468
MCSP0469




```

C      WRITE (6,153)
C      DO 62 K=1,NSAM
C      WRITE (6,155)
C      DO 62 I=1,N
C      WRITE (6,154) K,I,XM(I,K),ERR(I,K),VAR(I,I,K)
C      WRITE (6,156)
C      IF (I*STAT.EQ.0) GO TO 64
C      WRITE (6,157)
C      DO 63 K=1,NSAM
C      WRITE (6,158) K
C      DO 63 I=1,N
C      WRITE (6,146) (VAR(I,L,K),L=1,I)
C      CONTINUE
C      WRITE (6,156)
C      146  FORMAT (9(2X,1PE12.5),/)
C      147  FORMAT (1,20X,'OUTPUT DATA',//)
C      148  FORMAT (10X,'THE GAIN MATRICES ARE',/)
C      149  FORMAT (5X,'K=',I3,'/10X,'G(K)=',/)
C      150  FORMAT (1X,'/10X,'THE THEORETICAL COVARIANCE MATRIX IS',/)
C      151  FORMAT (5X,'K=',I3,'/10X,'P(K/K)=',/)
C      152  FORMAT (15,'SAMPLE MEAN OF',T16,'VECTOR COM-',T34,'SAMPLE MEAN',
C      153  1 T51,'SAMPLE INDEX',T16,'PONENT INDEX',T34,'CF TRACK',
C      154  1 T51,'ESTIMATION ERROR',T16,'ESTIMATION ERROR')
C      155  FORMAT (6X,I3,I3X,I1,10X,1PE14.7,2(6X,1PE14.7))
C      156  FORMAT (//)
C      157  FORMAT (10X,'THE SAMPLE COVARIANCE OF EST. ERROR MATRIX IS',//)
C      158  RETURN
C      END
C      SUBROUTINE PLT
C      REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
C      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,60),
C      3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
C      4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKM1(4),VIMP(4),Z(4),V(4),SIGV(4),
C      5XHATZ(4),XZ(60),YZ(60),PX(10),PY(10)
C      6N,NSAM,IQ,M,ITER,IIRK,IIN,I*STAT,K,I*TRD,IXZ,IV,IW,IEST,ND
C      DIMENSION ION XP(60),YP(60)
C      INTEGER*4 I*TB(12)/12*0/

```

MCSP0470
 MCSP0471
 MCSP0472
 MCSP0473
 MCSP0474
 MCSP0475
 MCSP0476
 MCSP0477
 MCSP0478
 MCSP0479
 MCSP0480
 MCSP0481
 MCSP0482
 MCSP0483
 MCSP0484
 MCSP0485
 MCSP0486
 MCSP0487
 MCSP0488
 MCSP0635
 MCSP0636
 MCSP0637
 MCSP0638
 MCSP0639
 MCSP0640
 MCSP0641
 MCSP0642
 MCSP0643
 MCSP0644
 MCSP0645
 MCSP0646
 MCSP0647
 MCSP0648

MCSP0878
 MCSP0879
 MCSP0880
 MCSP0881
 MCSP0882
 MCSP0883
 MCSP0885


```

REAL#4      RTB(28)/28*0.0/
EQUivalence (TITLE,RTB(5))
REAL#8      TITLE(12)/X = TRUE,  + = FILTER,  SQUARE = NOISY./
IGPLT=1
ITHVPL=1
ISMPLT=1
ISVPLT=1
DC 50 K=1, NSAM
XP(K)=XM(1,K)
YP(K)=XM(3,K)
CALL PLOTP(XP, YP, NSAM, 0)
ITB(1)=1
ITB(2)=1
CALL DRAWP(60, XP, YP, ITB, RTB)
DC 51 K=1, NSAM
XP(K)=XS(1,K)+ERR(1,K)
YP(K)=XS(3,K)+ERR(3,K)
CALL PLOTP(XP, YP, NSAM, 0)
ITB(1)=2
ITB(2)=2
CALL DRAWP(60, XP, YP, ITB, RTB)
ITB(2)=0
DO 2 J=1, 60, 5
IF (ABS(PKKS(1,1,J)-PKKS(3,3,J)).GT.0) GO TO 11
PKKS(1,1,J)=PKKS(3,3,J)+0.000001
CONTINUE
IF (0.5*ATAN(2.*PKKS(1,3,J)/(PKKS(1,1,J)-PKKS(3,3,J)))
THE=0.000001
CONTINUE
SIG2X=(PKKS(1,1,J)+PKKS(3,3,J))/2.+PKKS(1,3,J)/SIN(2.*THE)
SIG2Y=(PKKS(1,1,J)+PKKS(3,3,J))/2.-PKKS(1,3,J)/SIN(2.*THE)
WRITE (6,146) THE, SIG2X, SIG2Y
FORMAT (9(2X,1PE12.5),/)
SX=(SIG2X)**.5*20.
SY=(SIG2Y)**.5*20.
PT=3.14159265/12.
CT=COS( THE )
ST=SIN( THE )
DO 1 I=1, 25
XI=1
XP(I)=SX*COS( PT*XI)*CT-SY*SIN(PT*XI)*ST+XS(1,J)
YP(I)=SX*COS( PT*XI)*ST+SY*SIN(PT*XI)*CT+ XS(3,J)
CALL DRAWP(25, XP, YP, ITB, RTB)
ITB(1)=3
ITB(2)=3
CALL DRAWP(60, XZ, YZ, ITB, RTB)

```



```

C      DO 65 K=1,NSAM
C      65 XP(K) = K
C      IF (IGPLT.NE.1) GO TO 68
C      DC 67 I=1,N
C      DO 67 J=1,M
C      DO 66 K=1,NSAM
C      66 YP(K) = GKS(I,J,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      67 WRITE (6,159) I,J
C      68 IF (ITHVPL.NE.1) GO TO 71
C      DO 70 I=1,N
C      DO 69 K=1,NSAM
C      69 YP(K) = PKKS(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      70 WRITE (6,160) I,I
C      71 IF (IMTPLT.NE.1) GO TO 74
C      DO 73 I=1,N
C      DO 72 K=1,NSAM
C      72 YP(K) = XM(I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      73 WRITE (6,161) I
C      74 IF (ISMPLT.NE.1) GO TO 77
C      DO 76 I=1,N
C      DO 75 K=1,NSAM
C      75 YP(K) = ERR(I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      76 WRITE (6,162) I,I

```

```

MCSP0491
MCSP0492
MCSP0493
MCSP0494
MCSP0495
MCSP0496
MCSP0497
MCSP0498
MCSP0499
MCSP0500
MCSP0501
MCSP0502
MCSP0503
MCSP0504
MCSP0505
MCSP0506
MCSP0507
MCSP0508
MCSP0509
MCSP0510
MCSP0511
MCSP0512
MCSP0513
MCSP0514
MCSP0515
MCSP0516
MCSP0517
MCSP0518
MCSP0519
MCSP0520
MCSP0521
MCSP0522
MCSP0523
MCSP0524
MCSP0525
MCSP0526
MCSP0527
MCSP0528
MCSP0529
MCSP0530
MCSP0531
MCSP0532
MCSP0533
MCSP0534
MCSP0535
MCSP0536
MCSP0537
MCSP0538

```





.0001
.01

0.3333

.0001

10.
0.3333

.0001

10.



LIST OF REFERENCES

1. H. W. Sorenson, "Kalman Filtering Techniques," Advan. Control System, Vol. 3, Chapter 5, 1966.



INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Documentation Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0212 Naval Postgraduate School Monterey, California 93940	2
3. Chairman, Code 52 Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1
4. Professor H.A. Titus, Code 52Ts Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	18
5. Capt. Charles Dittmar Weapons and Systems Engineering United States Naval Academy Annapolis, Maryland	1
6. Assoc. Professor Donald E. Kirk, Code 52Ki Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1
7. Commander Naval Electronics System Command National City Washington D.C. 22030 ATTN: Charles Gill	2
8. Marine Corps Test and Evaluation Center Camp Pendleton, California ATTN: Major Norbert Spitzer	2
9. Robert R. Fossum Dean of Research (Code 023) Naval Postgraduate School Monterey, California 93940	1

Thesis

164323

D592

Dittmar

c.1

The application of
extended Kalman fil-
tering to the Position
Locating Reporting
System (PLRS).

thesD592

The application of extended Kalman filter



3 2768 001 89421 5
DUDLEY KNOX LIBRARY